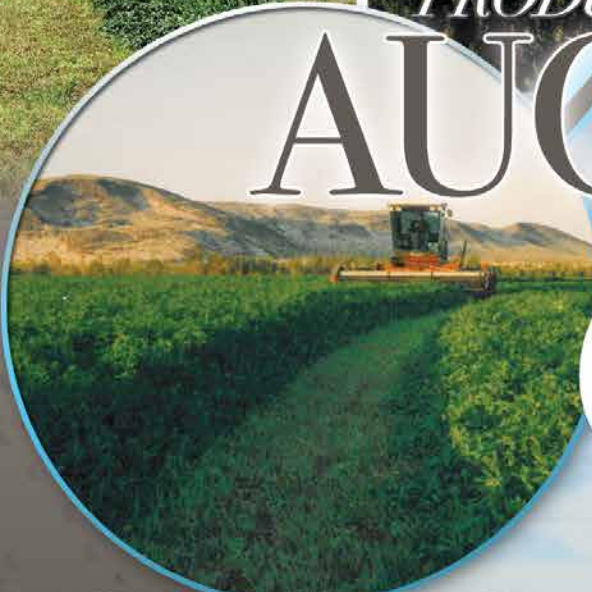


San Bernardino Co.,
California

LAND & ASSOCIATED WATER
PRODUCTION RIGHTS

AUCTION

640⁺
acres



Stock Photo



Stock Photo

California Aqueduct

- Water consultants have estimated between 20,000 to 30,000 acre feet per year
- Historic use of 10,000± acre feet per year
- 23 years of alfalfa production
- 7± Miles Northeast of Large Solar Plant
- Historically Known as Water Valley

SCHRADER
Real Estate and Auction Company, Inc.

in cooperation with

LEE & ASSOCIATES
COMMERCIAL REAL ESTATE SERVICES

Thurs., February 28 • 1PM

800-451-2709 • SchraderAuction.com

INFORMATION BOOKLET

V1.8

AUCTION COMPANY AND BROKER DISCLAIMER

This Information Booklet has been assembled on behalf of Curtis Jahnke and Ace Exploration and Water Drilling Company (collectively, the "Owner") for purposes of the auction to be conducted on February 28, 2013 by Schrader Real Estate and Auction Co., Inc. ("Auction Company") in cooperation with Lee & Associates Commercial Real Estate Services (the "Broker"). The information in this booklet consists of: (i) Owner-supplied historical information regarding the property; and (ii) third party information regarding legal, geological and hydrological information pertaining to the water rights (or excerpts thereof selected by the Owner for purposes of this booklet).

The Auction Company and Broker (collectively, "Owner's Representatives") are not qualified and have not undertaken to evaluate, interpret or vouch for any information or reports regarding any purported legal, geological or hydrological attributes of the water rights to be offered at auction. The Auction Company has attempted to identify the sources of the information provided herein. If there is any question regarding the source of any information, please contact the Auction Company for clarification.

The marketing materials prepared for this auction, including this Information Booklet, have been designed for prospective bidders who have (or have access to) the expertise necessary to independently evaluate the geological and hydrological attributes of the property and the legal issues relevant to the water rights offered for sale. Such marketing materials are not intended as a complete record of information pertaining to the property and water rights, nor are they intended as a substitute for a complete and independent investigation and evaluation by a prospective bidder and its qualified advisers. All prospective bidders are responsible for obtaining their own independent technical and legal advice and for conducting their own independent investigation and evaluation of the property and water rights offered at the auction and the information and reports provided with respect thereto.

OWNER'S REPRESENTATIVES MAKE NO REPRESENTATION OR WARRANTY REGARDING THE PROPERTY OR WATER RIGHTS. OWNER'S REPRESENTATIVES SHALL HAVE NO LIABILITY WITH RESPECT TO, AND HEREBY DISCLAIM ALL REPRESENTATIONS AND WARRANTIES CONTAINED IN, ANY INFORMATION OR REPORTS PROVIDED BY OWNER AND/OR THIRD PARTIES IN CONNECTION WITH THIS AUCTION.



SCHRADER REAL ESTATE & AUCTION CO., INC.
950 N. Liberty Dr., Columbia City, IN 46725
260-244-7606 or 800-451-2709
SchraderAuction.com



California Real Estate Broker:
Clifford Crowe, Principal
California Real Estate Broker
(License # 00982577)
1900 Wright Place Suite 200
Carlsbad, CA 92008

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MARKMAN LETTER



RICHARDS | WATSON | GERSHON
ATTORNEYS AT LAW – A PROFESSIONAL CORPORATION

1 Civic Center Circle, P.O. Box 1059, Brea, California 92822-1059
Telephone 714.990.0901 Facsimile 714.990.6230

February 15, 2006

RICHARD RICHARDS
(1916-1988)

GLENN R. WATSON
(RETIRED)

HARRY L. GERSHON
(RETIRED)

STEVEN L. DORSEY
WILLIAM L. STRAUSS
MITCHELL E. ABBOTT
GREGORY W. STEPANICH
ROCHELLE BROWNE
WILLIAM B. RUDELL
QUINN M. BARROW
CAROL W. LYNCH
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T. PETER PIERCE
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JANET E. COLESON
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BRUCE G. MCCARTHY
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GENA M. STINNETT
MATTHEW E. COHEN
ANDREW TAM

OF COUNSEL
MARK L. LAMKEN
SAYRE WEAVER
WILLIAM K. KRAMER
NORMAN A. DUPONT

LOS ANGELES OFFICE
TELEPHONE 213.626.8484

SAN FRANCISCO OFFICE
TELEPHONE 415.421.8484

VIA E-MAIL AND U.S. MAIL



Re: Response to Inquiry by [REDACTED] With Respect to the Legal Ability to Protect Water Production from the Jahnke Parcel

Dear [REDACTED]

I am addressing this letter to you in response to [REDACTED] inquiry of February 7, 2006 regarding our ability to secure the right to continue to produce water from the Jahnke Parcel. The point of departure in discussing the secure or permanent nature of a right to produce groundwater must concern the legal order of priority for producing different rights. It first must be noted that priorities are only relevant at a time where there is not enough water present in a groundwater basin to meet all of the water production demands placed on the basin. In other words, priorities are only relevant and rights to continue to produce water only are put at risk when there is a shortage of water from the source. If that occurs, the lower priority water production could be curtailed by Court order in order to establish a balance between water consumption and water supply and prevent the depletion of the resource.

The priorities, with an explanation of the types of rights discussed, are as follows:

1. Overlying Rights. Overlying rights are "locational" in nature. They are rights to produce water from property owned by one party to be used on property overlying the groundwater basin also owned by that party. Examples of overlying rights include farming in which the water supplied for the farming operation is produced from a parcel owned by the same entity which is operating the farm. Another example would be drawing water from a groundwater basin in order to provide cooling water for a power plant located on property overlying the same basin.

Source:

This letter was provided to Schrader Real Estate and Auction Co., Inc. by the Owner. Mr Markman has a financial interest in the sale of the property.

MARKMAN LETTER

RICHARDS | WATSON | GERSHON
ATTORNEYS AT LAW – A PROFESSIONAL CORPORATION

[REDACTED]
February 15, 2006

Page 2

2. Appropriative Water Rights. The appropriative water right is subordinate to the overlying water right. That is, in times of shortage, if only those two types of rights are present, the appropriative water right would have to be curtailed in order to balance consumption and water supply and protect the resource. An appropriative water right is a right exercised by one party producing water from property it owns (typically a retailer supplier such as a city or water district) and supplying that water to property owned by others (retail customers). The project which we have been discussing would establish an appropriative right to remove water from the basin and convey that water elsewhere for use by customers.

3. Priorities Among Appropriators. As among multiple appropriators pumping from land overlying the same groundwater basin, priorities are established by the principle of “first in time is first in right.” That is, the first appropriator to remove a certain amount of water from a groundwater basin and put it to beneficial use continues to have a right to do so paramount to the right of another appropriator who begins to appropriate water from the same groundwater basin at a later time.

4. Prescriptive Rights. There also is a type of right in California known as a prescriptive right. This right is established by water production during times of shortage which is adverse and hostile to production by parties with paramount rights. These types of rights typically are awarded in large groundwater basins where municipal pumping and agricultural pumping have competed within the same basin for a number of years. Prescriptive rights are not relevant to the project under discussion.

As mentioned above, the project we are considering would include the production of water utilizing appropriative water rights and not overlying water rights. Accordingly, there must be acknowledged at least some small degree of business risk of the project being blocked in later years by competing paramount production from overlying producers.¹ Please note that ongoing appropriative production still may be placed into a subordinate position by newly exercised overlying rights. In simple terms, it is possible that our established water production could later be blocked or reduced if enough overlying production is established in the groundwater basin to

¹ This also is the reason why it would be advantageous to utilize water extracted from the Jahnke parcel. If the water is extracted from another parcel, Mr. Jahnke is in the position to exercise his overlying production to its maximum capacity which could limit the amount of water available to be appropriated from any other parcel overlying the same basin.

MARKMAN LETTER

RICHARDS | WATSON | GERSHON
ATTORNEYS AT LAW - A PROFESSIONAL CORPORATION

February 15, 2006
Page 3

create a shortage which would require the appropriative production to be curtailed. Accordingly, while under circumstances known to us, this appears to be extremely unlikely, it is suggested later in this letter that further due diligence could occur during the period of time when the hydrologic investigation is occurring to rule out (insofar as it is possible to do so) the potential establishment of paramount production by overlying water producers.

The field observations which have occurred to date have disclosed only Mr. Jahnke as a water producer who presently is pumping available water from the basin. Further, if there had been a significant production by a party other than Mr. Jahnke and his company, Ace Well Drilling, such a party would have been identified and brought into the Mojave River Basin Water Adjudication. To our knowledge, no such person was identified. In that adjudication, all parties within the area being adjudicated (including the area under discussion) who were believed to produce more than 10 acre feet per year were included as defendants in the adjudication. Last week, I discussed the producers in the area north of Hinkley with Robert Wagner, Mojave Water Agency engineer. Mr. Wagner only could remember one water producer other than Mr. Jahnke north of Hinkley who was included in and now is bound by the Judgment in the Mojave Adjudication. That pumping was described as "miles south of Jahnke." Accordingly, at this time, all facts known to us provide a sound basis to believe that, other than Mr. Jahnke, no party owning property overlying the subject groundwater basin has produced significant water in the past or is now doing so.

The risk of competitive overlying pumping could be further assessed if deemed advisable through the following additional due diligence process:

1. Determine the surface area overlying the subject groundwater basin.
2. Identify present water producers other than Mr. Jahnke, if any, from that surface area and establish an amount of present production occurring, if any.
3. Assess whether that present production, if any, constitutes a threat to the viability of the project we are undertaking.
4. Examine all of the parcels overlying the water source as to size, zoning and ownership in order to assess with available data the likelihood of competing water production being established in the future.

MARKMAN LETTER

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[REDACTED]
February 15, 2006
Page 4

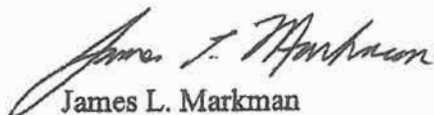
In summary, at present, the Jahnke production which is now overlying in nature and put to agricultural use is the only significant production from the basin which has been identified during the course of initial geologic investigations, field observations and review of Mojave Water Adjudication documentation. The project's production from the Jahnke parcel will be appropriative in nature and, to our present knowledge, will be first in time and first in priority as to appropriative use. It also would be free of competition from any significant overlying use known at this time. To provide further assurance and risk assessment, the above-referenced due diligence process could occur during the time when the hydrologic investigation is ongoing.

[REDACTED]
Redacted at author's request.

Finally, the project includes the construction of a pipeline to convey water from the Jahnke parcel to a point of delivery which meets the needs of water purchasers. Our ownership of and/or the sizing of the pipeline may preclude the use of the pipeline by any potential competitor. This would present a financial impediment to such a competitor who also would hold appropriative rights subordinate to ours.

I hope this information is responsive to [REDACTED] concerns.

Very truly yours,


James L. Markman
JLM/nlc

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MARKMAN RESUME

Professional Resume James L. Markman

James L. Markman is a shareholder in the Public Law Department and Water Rights and Water Law Practice Group at Richards, Watson & Gershon with more than 30 years of experience representing local public agencies. Mr. Markman is the Chair of the Water Rights and Water Law Practice Group and serves on the Firm's Management Committee.

Mr. Markman serves as special water rights counsel to California Domestic Water Company, a group of approximately 1,000 landowners in the Anza Valley in reference to a lawsuit involving tribal water rights, the Nipomo Community Services District regarding the Santa Maria Water Adjudication, the City of Palmdale in the Antelope Valley Water Adjudication, Marina Coast Water District and other public and private interests. He also serves as General Counsel to Mission Springs Water District and Beaumont-Cherry Valley Water District. Mr. Markman presently serves as City Attorney in the cities of Brea, La Mirada and Rancho Cucamonga.

Mr. Markman has been involved in many of the significant California groundwater adjudications which have occurred since 1969, including the Upper San Gabriel Basin, the Chino Basin, the Mojave River Basin, Six Basins (Claremont area), and the ongoing Santa Maria and Antelope Valley adjudications. Most recently, Mr. Markman argued on behalf of the public water suppliers in the Court of Appeals in the Santa Maria case.

Mr. Markman has been involved in virtually every significant groundwater adjudication which has occurred commencing in 1969, including the Chino Basin, Cummings Basin, Mojave River Basin, Six Basins, Upper San Gabriel and the ongoing Santa Maria and Antelope Valley adjudications.

Mr. Markman was a principal trial counsel and represented numerous public agencies in the Court of Appeals and the California Supreme Court in the successful second effort to adjudicate and bring management to the water resources of the Mojave River Basin. He now represents public agencies involved in active water negotiations and related matters in Los Angeles, San Bernardino, Orange, Riverside, Santa Barbara and San Luis Obispo Counties.

Source:

This resume was provided to Schrader Real Estate and Auction Co., Inc. by Mr. James L. Markman. Mr Markman has a financial interest in the property.

PROPERTY INFORMATION

A. Property Information

The Property consists of 640+- acres in Section 5 of Township 11 North, Range 3 West in San Bernardino County, State of California.

The property includes two Lindsay/Zimmatic irrigation systems on the eastern half of the property put up in approximately 2005. (The two irrigation systems on the western half of the property have been removed due to age.) Additional improvements include a 93'x200' hay barn, 50'x80' steel building with concrete floor used as a shop, a 3-bedroom home and a double-wide modular home.

The property has 3 unique features over almost any other property in the Mojave River Agency, an area roughly the size of Connecticut:

- 1) The property owner retains the legal right to pump water free of the restrictions imposed in the Mojave River Basin adjudication
- 2) The property lies at the mouth of the Black Canyon watershed, an area referred to as Water Valley (shown on map below)
- 3) There are few (if any) wells north of this property in the Black Mountain Wilderness Area

B. History of Oasis Ranch

Purchased in 1979, Curt Jahnke developed the 640 acres into a profitable alfalfa operation, raising alfalfa until 2006 with an average annual production of approximately 6,000 tons of alfalfa hay under 4 pivots. Water for the pivots came from 5 wells, producing an estimated 10,000 acre-feet per year for the cropland, 2 lakes created on the property, 20,000 trees, and 16 miles of additional trees bordering the property. The water in the lakes brought geese, ducks, and sandhill cranes, and the transformation was complete: the property truly became The Oasis Ranch. Due to health issues with Mrs. Jahnke in 2006, Mr. Jahnke was not able to continue the operations at Oasis Ranch.

C. 2011 Water Testing

In a 2011 Hydrogeologic Evaluation of the property, Well #3 was test pumped for 72 hours and had an average pumping rate of 1,621 gpm. During the 72-hour test, a total of about 7,000,000 gallons were pumped or 21.5 acre-feet. The five surrounding wells were monitored around the pumping well on the property showing a drawdown of 2 inches (from well 3,732 feet northeast of the pump) to 18 inches (from well 1,222 feet south of the pump) during the test. After 72 hours, the water level in the pumping well had drawn down about 27 feet. Within 6 seconds after turning the pump off the water level had risen to 77% of total recovery. One minute after turning the pump off, the water level had risen to 100 percent. (See Appendix B)

Source:

A & B: Owner

C: 2011 Ron Barto Ground Water Consultant report



2006 Photo



2006 Photo



2006 Photo



2006 Photo



Source:

Top photos were provided by the Owner and are believed to have been taken around 2006. Bottom photo was taken by Schrader Real Estate and Auction Co., Inc. on the property in December 2012.



Source:
Photos taken by Schrader Real Estate and
Auction Co., Inc. in January 2013.

GENERAL TERMS OF SALE

PROCEDURE; REGISTRATION: The Property will be offered as a total unit. The conduct of the auction and increments of bidding will be at the direction and discretion of the Auctioneer. Bidders can either preregister with the Auction Company on or before Thursday, February 21st, 2013 by submitting the preregistration form available on the Auction Company's website, or provide a bank letter of credit on the day of auction.

PURCHASE CONTRACT; SELLER'S ACCEPTANCE: The final bid price is subject to the Seller's acceptance or rejection. The successful bidder will be required to sign a purchase contract at the auction site immediately following the close of the auction. Copies of the purchase contract will be available prior to the auction upon request. The terms of the written purchase contract will supersede and take precedence over any prior statements or advertisements.

PROPERTY: The successful bidder at auction will purchase and acquire all of Seller's rights with respect to the Property, including:

- Surface rights, with existing improvements and irrigation equipment;
- Mineral, oil and solar rights;
- The **"First Tier Water Rights"** (i.e., the right to produce water from the Property up to and including 10,000 acre-feet in any calendar year); and
- The **"Additional Water Rights"** (i.e., the right to produce water from the Property in excess of 10,000 acre-feet in a calendar year).

Certain statements in the previously-printed auction brochure require clarification with regard to the water rights. All water production rights are included in the sale of the Property and will be acquired by the purchaser at closing. However, only the First Tier Water Rights will be included in the Bid Price paid at closing. The purchase price for the Additional Water Rights will be paid **post-closing** based on actual production volume over and above 10,000 acre feet per year.

PAYMENT OF BID PRICE; EARNEST MONEY: An earnest money deposit in the amount of 10% of the winning Bid Price will be due on the day of auction and the balance of the Bid Price will be due in cash at closing. The earnest money deposit may be paid in the form of a cashier's check, personal check, or corporate check. **YOUR BIDDING IS NOT CONDITIONAL UPON FINANCING**, so be sure you have arranged financing, if needed, and are capable of paying cash at closing.

ADDITIONAL WATER RIGHTS: The purchase price for the Additional Water Rights will be determined and paid in the manner and amounts and at the times set forth in the purchase contract, on the following basic terms:

- Water produced from the Property in any calendar year in excess of 10,000 acre-feet and up to 15,000 acre-feet shall be purchased as a permanent Additional Water Right at a price of \$5,500 per acre-foot. For example, if the purchaser/producer who previously had not produced water in a calendar year exceeding a volume of 10,000 acre-feet produces 12,002 acre-feet in a calendar year, that producer shall then pay to seller the sum of \$11,011,000.00 and shall have the permanent right to produce up to 12,002 acre-feet annually.
- 15,000 acre-feet up to 20,000 acre-feet shall be purchased as a permanent Additional Water Right at a price of \$6,500 per acre-foot.
- Production in excess of 20,000 acre-feet shall be purchased as a permanent Additional Water Right at a price of \$7,500 per acre-foot.
- The purchase price per acre-foot for Additional Water Rights shall be increased, on each January 1 following the fourth year subsequent to the auction, by the percentage increase in the Mojave Water Agency Replacement Water Assessment from January 1 of the previous year.
- Payment for Additional Water Rights produced shall be due on or before the March 1 immediately following the calendar year in which that production occurred. The payment shall be made together with accounting materials sufficient to document the amount of production which occurred in the previous calendar year. The payment and supporting materials shall be subject to audit by Seller at its discretion. The Purchase Agreement will contain more detailed provisions on payment for Additional Water Rights.

GENERAL TERMS OF SALE

POST-CLOSING AGREEMENTS: Seller has a substantial interest in the development of the full water production potential of the Property. Accordingly, the Purchaser shall be obligated to employ its best efforts to promptly conduct necessary studies to establish the maximum amount of water which can be produced from the Property and supplied for reasonable and beneficial uses and, upon establishing that amount, to continue to employ its best efforts to sell and provide that maximum amount of water through the applicable regulatory, construction and marketing processes. Those efforts shall include, but not be limited to, the following:

1. By July 1, 2014, complete a bore hole on the Property at least 3,000 feet in depth and 8” to 10” in diameter and produce a full detailed drill log with an explanation of materials drilled every 5 feet, a full E-log with commentary and a full temperature log every 50 feet; and
2. By January 1, 2016, complete the construction of two commercial production wells on the Property capable of producing 4000 GPM each with 1,000 feet of 24” casing with adequate Roscoe Moss louvered screening, in accordance with the specifications provided in this material.
3. Upon construction of the wells specified above, provide Seller with the results of a 72 hour minimum pump test of the wells (at a minimum of 7,000 gpm), monitoring all on-site wells, and, if possible, at least one well located off the Property to the south (e.g. well #7 mentioned in the Barto Report).

The Purchaser shall provide to Seller copies of all information concerning the Property and its water bearing capacity and water quality obtained by Purchaser, including all test results, reports and the product of computer models, generated by all tests performed on and investigations of the Property together with the consideration of other available data.

DELIVERY OF TITLE; TITLE INSURANCE: Seller will deliver title and provide title insurance in accordance with the terms and conditions of the purchase contract. The cost of title insurance will be shared equally (50:50) by Seller and Buyer.

CLOSING; POSSESSION: The closing will be held as and when provided in the purchase contract. The closing agent’s fee for administering the closing will be shared equally (50:50) by Seller and Buyer. Possession will be delivered at closing.

PROPERTY TAXES: Buyer will assume the property taxes beginning with those assessed for the calendar year 2013. All prior property taxes will be paid by Seller at or prior to closing or via credit to Buyer at closing. **UPDATE:** The property taxes will not be pro-rated (notwithstanding the terms stated in the previously-printed auction brochure).

SURVEY; ACREAGE: The Property will be conveyed using existing legal descriptions, without a new survey. All tract acreages, dimensions and boundaries stated or depicted in the marketing materials are approximate and have been estimated based on existing legal descriptions and/or aerial photos.

AGENCY: The Auction Company and Broker and their respective agents and representatives are exclusively the agents of the Seller.

DISCLAIMER AND ABSENCE OF WARRANTIES: THE PROPERTY IS BEING SOLD “AS IS, WHERE IS”. SELLER, BROKER AND AUCTION COMPANY MAKE NO WARRANTY OR REPRESENTATION, STATED OR IMPLIED, CONCERNING THE PROPERTY. Prospective bidders are responsible for conducting their own independent inspections, investigations, inquiries, and due diligence concerning the Property. The Seller, Broker and Auction Company assume no responsibility or liability for errors or omissions. The Seller and its representatives reserve the right to preclude any person from bidding if there is any question as to the person’s credentials, fitness, etc. All decisions of the Auctioneer are final with regard to the conduct of the auction.

CHANGES: These general terms are subject to change. Check the auction website for updates at www.schraderauction.com. The terms of the written purchase contract, written auction day announcements, and/or official announcements made at the auction podium during the auction will supersede and take precedence over any other terms, statements or advertisements, whether oral, in print, or posted to the auction website.

BEEBY ENGINEERING CALCULATIONS

BEEBY ENGINEERING, INC.

OASIS RANCH		
Miscellaneous Calculations		
POTENTIAL WATER SUPPLY ^(a)		
Area of Harper Lake Basin (from 2007 CSUF report)	678 Square Miles or 433,920 Acres	
Average precipitation (from 2007 CSUF report)	5.2 Inches	
Total volume of precipitation	188,032 Acre-Feet	
Volume of precipitation contributing to Oasis Ranch		
	Percent of HLB contributing to Oasis Ranch	Annual Gross Volume
	10%	18,803 Acre-Feet
	15%	28,205 Acre-Feet
	20%	37,606 Acre-Feet
	25%	47,008 Acre-Feet
<p>(a) The water supply that potentially contributes to the sustainable supply available to Oasis Ranch is estimated by multiplying the surface area (as a percentage of the total) by the average annual precipitation. Some of the precipitation falling on the contributing area will be used by native vegetation and evaporated from the soil surface but for purposes of this calculation, it is assumed that most runs off from the basalt mountains and percolates to the underlying alluvium or fractured bedrock underlying the Ranch. This is based on the fact that the types of storms are short-duration and high intensity. The estimate may be conservative because the average annual precipitation is for Barstow and the elevations of the Black Mountain region is higher than Barstow and precipitation is likely greater than at Barstow.</p>		

Source:

The charts in this section were provided to Schrader Real Estate and Auction Co., Inc. by the Owner. Beeby Engineering, Inc. described the contents as follows:

These calculations were prepared by Beeby Engineering, Inc. at the initial stage of the appraisal-level investigation of the water supply potential of the Oasis Ranch. The purpose was to check and to illustrate the reasonableness of information provided by Mr. Jahnke. The calculations essentially confirmed the figures provided by Mr. Jahnke and were later discussed and provided to interested parties, including technical experts retained to investigate the hydrogeologic aspects of the Oasis Ranch and to the Mojave Water Agency and their professional staff.

Beeby Engineering, Inc. and/or Bob Beeby has a financial interest in the sale of the property.

BEEBY ENGINEERING CALCULATIONS

BEEBY ENGINEERING, INC.

OASIS RANCH

Miscellaneous Calculations

ESTIMATED POTENTIAL ANNUAL PRODUCTION

Estimated Production Rates per Well	Acre-Feet Produced at Various Annual Operational Percentages		
	90%	80%	70%
1,500 gpm	2,200	1,900	1,700
2,000 gpm	2,900	2,600	2,300
2,500 gpm	3,600	3,200	2,800
3,000 gpm	4,300	3,900	3,400

Wells required to produce 10,000 Acre feet per year

Estimated Production Rates per Well	Number of Wells Required at Various Annual Operational Percentages		
	90%	80%	70%
1,500 gpm	5	6	6
2,000 gpm	4	4	5
2,500 gpm	3	4	4
3,000 gpm	3	3	3

Wells required to produce 12,000 Acre feet per year

Estimated Production Rates per Well	Number of Wells Required at Various Annual Operational Percentages		
	90%	80%	70%
1,500 gpm	6	7	8
2,000 gpm	5	5	6
2,500 gpm	4	4	5
3,000 gpm	3	4	4

Wells required to produce 30,000 Acre feet per year

Estimated Production Rates per Well	Number of Wells Required at Various Annual Operational Percentages		
	90%	80%	70%
1,500 gpm	14	16	18
2,000 gpm	11	12	14
2,500 gpm	9	10	11
3,000 gpm	7	8	9

BEEBY ENGINEERING CALCULATIONS

BEEBY ENGINEERING, INC.

OASIS RANCH				
Miscellaneous Calculations				
WATER DEMANDS (Theoretical-based on Areas and ET)				
Gross acreage	160 x 4 =	640	acres	
Center pivot with end gun	156 x 4 =	624	acres	
Center pivot with no end gun	126 x 4	503	acres	
Irrigated windbreaks	5240 x 10 x 3 =	4	acres	
Pond	600 x 100 =	1.4	acres	
Theoretical Annual Applied Water Demand (Pumpage)				
	Item	Unit Pumpage	Acre-feet per Year	Acre-feet per Year ⁽¹⁾
	Alfalfa	7.0	4,370	3,520
	Windbreaks	5.5	20	20
	Pond	7.0	10	10
	Total		4,400	3,550
⁽¹⁾ No end gun on alfalfa fields				
Estimated Annual Pumpage (based on Owners operating information)				
	Well	Production (GPM)	Operating Time	Acre-feet per Year
	Well #1	1,300	92%	1,940
	Well #2	1,300	92%	1,940
	Well #3	1,125	92%	1,680
	Well #5	1,600	92%	2,380
	Test Well	800	92%	1,190
			Total	9,130
Note: Operating time based on no irrigation for four days following the seven cuttings/year or 28 days without irrigation/yr.				

Table for Aerial photo showing well locations

OASIS RANCH WELL DATA							
	Well	#1	#2	#3	#4	#5	Test
	Drilled	1979	1983	1983	1983	1995	1979
	Depth	207	345	206	252	410	355
	Perfs	?	95-345	?	95-143	205-405	55-355
	gpm	1,300	1,300	1,125	Not used	1,600	800

BARTO REPORT EXCERPTS

Excerpts from Hydrogeologic Evaluation July 2011

TABLE 1
Summary of Well Construction and Water Level Data

	Units	WELL - 1	WELL - 2	WELL - 3	WELLS - 4	WELLS - 5	WELL - 6
Borehole Diameter	Inch	12	-	24	24	-	32/14
Casing Diameter	Inch	8	14	14	14	14	18/10
Casing Material		Steel	Steel	Steel	Steel	Steel	Steel
Borehole Depth	Feet	355	207	345	363	215	410
Casing Depth	Feet	355	207	345	252	215	405
Perforated interval	Feet	55 - 355	-	95 - 345	95 - 363 252 ^A	-	140 - 405
Surface Seal	Feet	-	-	0 - 20	0 - 20	-	0 - 40
Date Drilled		10/4/1979	10/22/1979	5/23/1983	Mar-83	-	7/5/1995
Ground Surface Elevation*	Feet	2062	2077	2066	2084	2073	2072
Reference Point Elevation*	Feet	2062	2079	2067	2085	2074	2072
Depth to Water when Drilled	Feet	49 ^B 40	58	47	68	55	-
Depth to Water on Feb. 28, 2011	Feet	69.0	82.3	74.0	91.2	80.0	76.6
Water Surface Elevation*	Feet	1993.0	1996.7	1993.0	1993.8	1994.0	1995.4

*Ground Surface Elevations based on Google Earth Data

^A **Owner's Comment:** Believed to be 252 based on casing depth

^B **Owner's Comment:** Believed to be 49, based on drill log

Source:

This section consists of excerpts from a Hydrogeologic Evaluation prepared by Ron Barto Ground Water Consultant in 2011, and provided to Schrader Real Estate and Auction Co., Inc. by the Owner. Owner's comments appear in red. Some text has been made bold and highlighted. The full report is available by contacting Schrader.

BARTO REPORT EXCERPTS

Google Earth data were used to determine the ground surface elevation at each of these wells. It is not clear as to the accuracy of Google Earth data but probably is within 1 or 2 feet accuracy. The approximate ground surface, reference point, and ground water surface elevations are shown in **Table 1**. It should be noted that distances between wells were also determine from Google Earth aerial photos. The accuracy of these horizontal distances is less critical to the analysis of gradient and is believed to be acceptable without further measuring and surveying.

The scope of this investigation did not include any land surveying to determine ground surface and reference point elevations. However, it now appears that such information is critical to the understanding of the on-site ground water gradient. Surveying of ground and reference point elevations should be included in the next investigation of Oasis Ranch.

From the available data collected during this investigation, it is apparent that ground water beneath the site flows in a southerly direction from Well # 2 to Well #3 at a gradient of about 0.16 percent (3.7 feet/2358 feet). There is also a southwesterly direction of flow, as evidenced by a 0.05 percent (1.0 feet/1824 feet) gradient between Well #5 and Well #3.

Although the accuracy is highly questionable, there is a slight southwesterly direction of flow between Well #4 and Well #3 at a gradient of about 0.02 percent (0.8 feet/3732 feet). Well #4 encountered a lot of clay and may not reflect true ground water levels in the area.

These data are only as good as the ground surface elevations and reference point elevations assumed for this investigation. Clearly, there are some questions about the reliability of these data. Preparing a ground water contour map of the property seemed futile at this time because of the accuracy of elevations used.

Based upon the ground water level elevation data collected and assumptions made in terms of elevations, ground water beneath the site flows in the southwesterly direction similar to that described earlier under regional hydrogeology. The on-site data show a gradient ranges between 0.05 and 0.16 percent.

BARTO REPORT EXCERPTS

ON-SITE AQUIFER WELL TEST

As part of this investigation, we conducted a 72-hour continuous aquifer pumping test on Well #3, and used the other five production wells on the property as monitoring wells. Well #3 is located in the center of Field 2 in the southwestern quarter of the Subject Property. The 10-inch diameter test pump was set at a depth of 190 feet with the top perforations in the well at 95 feet deep. A top gear head drive and portable diesel engine provided the power for the test. The 72-hour pumping test was followed by a 22-hour period of recovery. Pressure transducers were installed in each of the five monitoring wells. Depths to water in the five monitoring wells ranged between 69 and 91 feet deep, as detailed in **Table 1**.

WELL TEST

The well test was performed on Monday, February 28, 2011, through Friday, March 4, 2011. On the day of the test, the static water level in the pumping well was 74 feet below the top of the casing. Excessive oil in the pumping well floating on top of the water and the small annular space between the pumping column and the well casing made more accurate measurements impossible.

The test consisted of turning on the pump at 1:00 PM for a period of 72 hours of continuous pumping and measuring both the decline in water levels and the discharge over time. An in-line flow meter was used to measure the discharge of the pump. An electric probe was used to measure the depths to water in the pumping well. After the pump test was completed, the water level was allowed to recover. Recovery was monitored for an additional ten minutes when the well had recovered 100 percent.

The data collected during the pumping test are presented in **Appendix B**. A graph showing water level drawdown time pumped in the monitoring wells is shown in **Figure 12**.

BARTO REPORT EXCERPTS

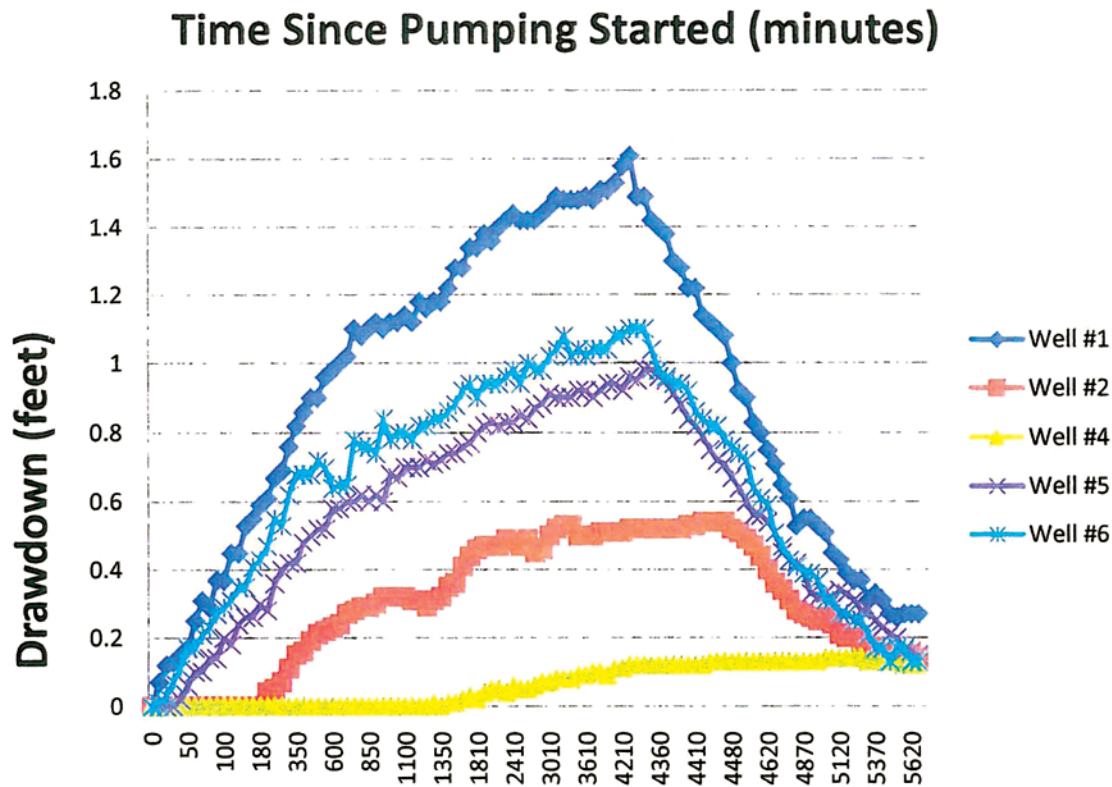


Figure 12 - Water Level Drawdown with Time

The graph clearly shows that the closer the monitoring well is to the pumping well, the quicker the well responds and the greater the amount of drawdown with time. It should be pointed out that the timescale across the bottom of the graph is not evenly spaced but shows greater spacing for time intervals at the beginning of the drawdown and again at the beginning of the recovery. Evenly spaced time intervals, known as rectangular plots, will appear that the drawdown is flat and has reached equilibrium by the end of the test. In reality, water levels continued to decline over time pumped but it takes increasingly longer periods of time to observe this decline. Semi-log plots of drawdown versus time frequently show a straight line water level decline. Such plots are useful when projecting drawdown over time pumped. Semi-log plots of these pump test data are presented in **Appendix B**.

The discharge rate from Well #3 averaged 1621 gpm. During the 72-hour test, a total of about 7,000,000 gallons were pumped or 21.5 acre-feet.

BARTO REPORT EXCERPTS

TEST RESULTS

As would be expected, the water level in the well drew down quickly at the beginning of the test, but slowly flattened off as pumping continued. After 72 hours, the water level in the pumping well had drawn down about 27 feet, to a depth of 101 feet below the top of the casing. After the pump was turned off, the water level rose rapidly to full recovery. **One minute after turning the pump off, the water level had risen to a depth of 74 feet; or 100 percent of total recovery was obtained within one minute after pumping terminated.**

The testing has shown that this well is a good producing well capable of yielding in excess of 1600 gallons per minute. No boundary effects were detected. While the well was being redeveloped for this test, **the contractor reported a short-term yield of 2500 gpm. As shown by the modest amount of drawdown, this well should be capable of yielding many more gallons per minute, say, 1800 to 2000 gpm, if a larger pump and motor were installed.** However, well production is limited by the size of the 14-inch diameter casing.

All five of the monitoring wells responded to the pumping of Well #3. The closest wells (Wells #1 and #6) responded almost immediately upon turning on the pump. Likewise, they had the greatest amount of drawdown at 1.6 feet and 1.1 feet, respectively. The test results are summarized in **Table 2.**

**TABLE 2
SUMMARY OF 72-HOUR WELL TEST**

	Units	WELL - 1	WELL - 2	WELL - 3	WELL - 4	WELL - 5	WELL - 6
Distance from Pumping Well	Feet	1222	2358	1	3732	1824	1386
Change in One Log Cycle	Feet	0.73	0.43	0.4	0.2	0.49	0.48
Time the Reach Well	Minutes	24	58	-	1300	39	20
Transmissivity	GPD/foot square	586,000	995,000	1,070,000	2,140,000	873,000	892,000
Storativity	Unit Less	0.002	0.002	-	0.04	0.002	0.002

Transmissivity is a measure of the aquifer's ability to transmit water. It is defined as the rate of flow in gallons per day through a vertical section of the aquifer whose height is the thickness of the aquifer and whose width is one foot, where the hydraulic gradient is 1.0. From the test pumping data, it was determined that the pumping well (Well #3) has a transmissivity value of about 1,070,000 gpd/ft (**Appendix B**). Permeability times the aquifer thickness equals

BARTO REPORT EXCERPTS

transmissivity. The alluvial thickness in this well is 214 feet* (depths from 74 to 288 feet); the permeability is calculated at about 5000 gallons per day per square foot. As shown in Table 3, transmissivity and permeability values in this range would be considered to be excellent when compared to other sand and gravel aquifers. Transmissivity values of the monitoring wells ranged between 586,000 and 2.1 million gpd/ft but mostly between 800,000 and 1 million gpd/ft. For this evaluation, the transmissivity value of the aquifer beneath the Oasis Ranch is considered to be 900,000 gpd/ft. This value is the average of the pumping well and the four closest monitoring wells. As discussed later, there appears to be something wrong with the data collected from Well #4, possibly because it encountered a lot of clay.

* **Owner's Comments:** Mr. Jahnke believes that, in addition to the stated 214-foot alluvial thickness, there is 200± feet of porous lava rock which, according to Mr. Jahnke, would double permeability.

Table 3
Magnitude of Permeability for Different Classes of Soils (Todd, 1959)

Permeability	Flow	Soil
(gal/day/sf)	Characteristics	Class
10 ⁶	Excellent Aquifer	Clean Gravel
10 ⁵	Excellent Aquifer	Clean Gravel
10 ⁴	Good Aquifer	Clean Sand, Mixture of Clean Sand and Gravel
10 ³	Good Aquifer	Clean Sand, Mixture of Clean Sand and Gravel
10 ²	Good Aquifer	Clean Sand, Mixture of Clean Sand and Gravel
10	Poor Aquifer	Very Fine Sand, Silt, Mixtures of Sand, Silt, and Clay
1	Poor Aquifer	Very Fine Sand, Silt, Mixtures of Sand, Silt, and Clay
10 ⁻¹	Poor Aquifer	Very Fine Sand, Silt, Mixtures of Sand, Silt, and Clay
10 ⁻²	Poor Aquifer	Very Fine Sand, Silt, Mixtures of Sand, Silt, and Clay
10 ⁻³	Impervious	Unweathered Clay
10 ⁻⁴	Impervious	Unweathered Clay

The specific capacity (SC) of the pumping well at the end of the test was about 60 gpm/ft (1641 gpm/27 feet drawdown). A SC value of 60 gpm/ft shows that well is an "alluvial" well.

Storativity (S) is defined as the volume of water that an aquifer releases or takes into storage per unit surface area of aquifer per unit change in head perpendicular to that surface. In confined aquifers, storativity values range between 0.005 and 0.00005 dimensionless units. In unconfined aquifers, storativity corresponds to the well's specific yield and range between 0.25 for gravel to about 0.03 for clay-rich soils. Storativity values ranging between 0.03 and 0.005 are defined as semi-confined conditions. From data collected during this test from five monitoring wells, the aquifer has a storativity value of about 0.040 to 0.003, making it semi-confined conditions.

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RECOVERY TEST

After the well was turned off, the water level was allowed to recover. Typically, well recovery is a mirror image of the drawdown. That is to say, if it takes 72 hours to draw the water level down in the well, it will take 72 hours plus a little bit more for the well to recover to its previously pumped water level. However, in every well, recovery was faster than drawdown, indicating a positive recharge to the area. As mentioned previously, **the pumping well recovered in an unbelievable 1 minute to its pre-pumped levels.** This rapid recovery was probably due to the pump column flowing back into the well but 10 minutes after stopping the pump, the water level remained at 74 feet. **Table 4** presents a comparison of drawdown and recovery at comparable time intervals.

TABLE 4
Comparison of Drawdown and Recovery During Well Test

	Units	WELL - 1	WELL - 2	WELL - 3	WELL - 4	WELL - 5	WELL - 6
Pumping Drawdown	60 min.	0.25	0	27	0	0.10	0.17
Recovery	60 min.	0.31	0	27	0	0.08	1.6
Pumping Drawdown	120 min.	0.45	0		0	0.24	0.35
Recovery	120 min.	0.51	-0.02		-0.01	0.25	0.32
Pumping Drawdown	400 min.	0.86	0.16		0	0.48	0.68
Recovery	400 min.	0.96	0.18		-0.01	0.51	0.63
Pumping Drawdown	750 min.	1.10	0.28	28	0	0.60	0.78
Recovery	750 min.	1.16	0.31		-0.02	0.65	0.79
Pumping Drawdown	1000 min.	1.12	0.32	26	0	0.68	0.78
Recovery	1000 min.	1.30	0.35		-0.01	0.68	0.89
Pumping Drawdown	1350 min.	1.18	0.32	27	0.01	0.72	0.84
Recovery	1350 min.	1.34	0.40		0	0.81	0.97

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LONG-TERM PUMPING

One of the benefits of pump testing is to be able to project drawdown of the water table in the future. By plotting pump test data on semi-log paper, drawdown can be estimated at some later date (**Appendix B**). **Table 5** presents the actual collected data, along with the projected drawdown amounts in each of the monitoring wells for a period of up to one year of continuous pumping. Clearly, projections of future data are prone to errors the further out you go on the time projection. Estimation of drawdown after 10 days is relatively accurate as long as pumping conditions stay relatively the same. However, projecting drawdown levels for three months, let alone one year, could produce highly variable results. The following projected information included in the “summary of drawdown versus time data” are estimates only and should be used as such.

TABLE 5
Summary of Drawdown versus Time Pumped at 1621 GPM

	Units	WELL - 1	WELL - 2	WELL - 3	WELL - 4	WELL - 5	WELL - 6
Distance from Pumping Well	Feet	1	1222	1386	1824	2358	3732
One Half Day	Feet	26.7	1.0	0.8	0.6	0.3	0.0
One Day	Feet	26.8	1.2	0.9	0.7	0.4	0.0
Three Days	Feet	27.0	1.6	1.1	1.0	0.5	0.1
Ten Days*	Feet	27.2	2.1	1.4	1.2	0.8	0.2
Three Months*	Feet	27.6	2.7	1.8	1.7	1.2	0.4
One Year*	Feet	27.7	3.2	2.1	2.0	1.4	0.5

* =Straight line projection of pump test data

If more than one well were pumped at a time, mutual interference would compound the drawdown in each well. If all six wells were continuously pumped at one time for one year, the resulting effect would be a theoretical drawdown of about 37 feet in each well ($27.7' + 3.2' + 2.1' + 2.0' + 1.4' + 0.5' = 36.9'$), assuming each pumping about 1600 gpm. Under such an operation, the total production would be about 8000 gpm or 12,800 acre-feet per year. This assumes that all the other five wells have the same well and aquifer characteristics as the tested well.

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STORAGE

Ground water in storage beneath the Oasis Ranch was determined by multiplying the surface area of the Ranch by the average saturated alluvial thickness by the specific yield of the saturated soils.

- Oasis Ranch covers approximately 640 acres.
- By applying specific yield values (**Table 6**) for the soil materials encountered in the saturated zone of each well log, the average specific yield for each well was determined. As shown on **Table 7**, specific yield ranged from 4.6 to 13.6 percent with an average of the five wells being 9.9 percent.
- By using the on-site well logs and the current depths to water, the current saturated alluvial thickness ranges between 125 and 276 feet, and averages at 174 feet thick (**Table 7**).

Storage was calculated using a specific yield of 9.9 percent, an average saturated alluvial thickness of 174 feet over the 640 acre ranch. Thus, the amount of ground water stored in the saturated alluvium beneath oasis ranch is about 11,025 acre-feet. Although the black lava bedrock may have water stored within it, it is considered non-water bearing and was not counted as part of the ground water in storage.

Table 6
Specific Yields of Water Bearing Deposits (Todd, 1959)

Materials	Specific Yield
	(Percent)
Gravel	25
Sand, Sand and Gravel, Gravel and Sand	20
Fine Sand, Hard Sand, Tight Sand, Sandstone	10
Clay and Gravel, Gravel and Clay, Cemented Gravel	5
Clay, Silt, Sandy Clay, Lava Rock, Fine Grained Deposits	3

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Table 7
Summary of Depth to Bedrock and Saturated Alluvial Thickness

Well #	Depth to Bedrock *(Volcanic Material) (ft)	Depth to Water (ft)	Saturated Thickness (ft)	Specific Yield (percent)
1	345	69	276	12.2
2	207	82	125	13.6
3	288	74	214	12.1
4	245	91	154	7.1
5	215	80	135	
6	214	76	138	4.6
Average	253		174	9.9

* **Owner's Comment:** Mr. Jahnke believes this column refers to the depth to Volcanic Material/ Lava Rock instead of Bedrock which, according to Mr. Jahnke could significantly increase the ground water flow calculation. See also Owner's previous comment regarding alluvial thickness and permeability.

SITE RECHARGE

To calculate the site recharge or the amount of ground water flow beneath Oasis Ranch, the data gleaned from this investigation is applied to Darcy's law as follows:

$$Q = TIW$$

Where T = transmissivity, in gpd/ft

I = ground water gradient, in ft/ft

W = width the flow of the property, in ft

The transmissivity value determined from the on-site pump test was used in Darcl's equation. However, the ground water gradient that was determined during this investigation differs from that determined during the previous more regional investigations by the USGS and the MWA-Cal state Fullerton. Therefore, both values are entered to determine the range of values for ground water flow beneath the Oasis Ranch. Although the property is one mile square, flow beneath the property is in a southwesterly direction, so the width of the property would be more on the diagonal or approximately 7400 feet long.

By using the on-site gradient of 0.16 percent:

$$\begin{aligned} Q &= (900,000) (0.0016) (7400) \\ &= 10,656,000 \text{ gpd} \\ &= 11,900 \text{ acre-feet per year} \end{aligned}$$

By using the regional gradient of 0.32 percent:

$$\begin{aligned} Q &= (900,000) (0.0032) (7400) \\ &= 21,300,000 \text{ gpd} \\ &= 23,900 \text{ acre-feet per year} \end{aligned}$$

That is to say, under current conditions, approximately 12,000 to 24,000 acre-feet of ground water flows naturally beneath the property each year.

BARTO REPORT EXCERPTS

ON-SITE WATER QUALITY

Water samples were collected from the pumping well (Well #3) on February 28, 2011, after five hours of pumping and again on March 2, 2011, after 72 hours of pumping. Samples were delivered to Clinical laboratory of San Bernardino, Inc. for general mineral and inorganic mineral content. Results of these analyses are summarized in Table 8. For easy comparison, this table also presents the maximum allowable limit or maximum concentration limit (MCL) for drinking water quality standards.

With the exception of fluoride and arsenic, none of the constituents in the pumping well exceeded the MCL for drinking water standards.

Table 8
Summary of Well #3 Water Quality

		Units	Max. Limit	Oasis Ranch 5 Hours	Oasis Ranch 72 Hours
CATIONS					
Hardness	(total)	mg/l		63	61
Calcium	(Ca)	mg/l		20	24
Magnesium	(Mg)	mg/l		6	6
Sodium	(Na)	mg/l		200	190
Potassium	(K)	mg/l		6	6
ANIONS					
Alkalinity	(total)	mg/l		190	180
Carbonate	(CO3)	mg/l		ND	ND
BiCarbonate	(HCO3)	mg/l		230	220
Sulfate	(SO4)	mg/l	500	160	160
Chloride	(Cl)	mg/l	500	130	130
Nitrate	(as NO3)	mg/l	45	4	4
Fluoride	(F)	mg/l	2	2.6	2.7
pH		stand. Units		8.1	8.1
Spec. Cond.	(EC)	us	1600	1100	1100
Total Filterable Residue	(TFR)	mg/l	1000	710	680
Methylene Blue Active Subs	(MBAS)	mg/l	0.5	ND	ND
Perchlorate	(ClO4)	ug/l	6	ND	ND
INORGANICS					
Aluminum	(Al)	ug/l	200	ND	ND
Antimony	(Sb)	ug/l	6	ND	ND
Arsenic	(As)	ug/l	10	90	84
Barium	(Ba)	ug/l	1000	ND	ND
Beryllium	(Be)	ug/l	4	ND	ND
Boron	(B)	ug/l		2700	2800
Cadmium	(Cd)	ug/l	5	ND	ND
Chromium	(Cr total)	ug/l	50	ND	ND
Copper	(Cu)	ug/l	1000	ND	ND
Cyanide		ug/l	150	ND	ND
Iron	(Fe)	ug/l	300	ND	ND
Lead	(Pb)	ug/l		ND	ND
Manganese	(Mn)	ug/l	50	ND	ND
Mercury	(Hg)	ug/l	2	ND	ND
Nickel	(Ni)	ug/l	100	ND	ND
Nitrate + Nitrite (as N)	(N)	ug/l	10000	940	890
Selenium	(Se)	ug/l	50	ND	ND
Silver	(Ag)	ug/l	100	ND	ND
Thallium	(Tl)	ug/l	2	ND	ND
Vanadium	(Vn)	ug/l		79	73
Zinc	(Zn)	ug/l	5000	ND	ND
				ND= Not Detected	

National Primary Drinking Water Regulations (NPDWRs or primary standards) are legally enforceable standards that apply to public water systems. Primary standards protect public health by limiting the levels of contaminants in drinking water. The EPA also establishes National Secondary Drinking Water Regulations as a non-mandatory water quality standard. EPA does not enforce the Secondary Standards; they are established only as a guideline for aesthetic considerations. These contaminants are not considered a health risk.

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As can be seen, the water quality changed very little during the 72 hour well test. The ground water of this well is of good quality with total dissolved solids (TDS) being 680 to 710 mgjl. Total dissolved solids, also referred to as total filterable residue (TFR), is a measure of the total salts dissolved in water. These consist chiefly of carbonates, bicarbonates, chlorides, sulfates, phosphates, and possibly nitrate, magnesium, sodium, and potassium. By comparison, distilled water has a TDS concentration of zero while "Arrowhead Drinking Water" pride themselves on bottling a very high quality and extremely low TDS concentration of about 200 mgjl. Colorado River water imported to southern California typically has TDS concentrations ranging from about 510 to 660 with an average of about 660 mgjl (MWD 2009 Annual Report). The maximum secondary concentration limit (SMCL) for TDS is set at 1,000 mgjl. TDS concentrations are well below the standard of 1000 mgjl set by the USEPA for Secondary Safe Drinking Water Standards. This limit was set primarily on the basis of taste thresholds.

Excessive fluoride concentrations are common throughout the desert regions. Fluoride concentrations in this well were measured at 2.6 and 2.7 mgjl, which are above the MCL of 2.0 mgjl limit set by the State for drinking water standards but significantly less than the 4.0 mgjl federal limit. "Fluoride in sufficient quantity is toxic to humans, with doses of 250 to 450 mg giving severe symptoms and 4.0 grams causing death" (McKee and Wolf, 1963). Abundant literature is also available describing the advantages of maintaining 0.8 to 1.5 mgjl of fluoride in drinking water to aid in the reduction of dental decay, especially among children. There is evidence that fluorides in excess of 5 mgjl can result in mottling of teeth. No other harmful effects are reported for excessive fluoride in drinking water. The amount of fluoride at the subject site is not considered a serious health concern.

Arsenic concentrations are also common throughout the desert regions. Samples taken during the Well #3 testing showed 90 ugjl after five hours of pumping and had declined slightly to 84 ugjl after 72 hours of pumping, with a primary standard of 10 ugjl. Arsenic occurs naturally in rocks, soil, water, air, plants, and animals. Levels are generally higher in the western States due to geologic conditions. Arsenic can be spread through the environment by natural processes, such as erosion and forest fires, and human activities, such as mining and agriculture. Because of their contact with naturally occurring underground rock formations, ground waters tend to have higher levels of arsenic than surface waters. "Arsenic is notorious for its toxicity to humans. Ingestion of as little as 100 mgjl usually results in severe poisoning. Furthermore, arsenic accumulates in the body, so small doses may become fatal in time. A single dose may require ten days for complete disappearance and this slow excretion is the basis for the cumulative toxic effect" (McKee and Wolf, 1963). Some people who drink water containing arsenic in excess of the MCL over many years could experience skin damage or problems with their circulatory system, and may have an increased risk of getting cancer.

For many years, the mandatory limit for arsenic in drinking water was 0.05 mgjl (50 ugjl), but recently the limit for arsenic was lowered to 10 ugjl. If this water from Oasis Ranch is to be used for drinking water in the future, treating water to reduce arsenic will be necessary if more cost-effective alternatives, such as blending, are not available. EPA has identified best available technologies (BATs) and small system compliance technologies (SSCTs) for removing arsenic from drinking water. EPA anticipates that most small systems will use activated alumina (or another type of adsorptive media), reverse osmosis devices, or modified lime softening. Most technologies may require pre-treatment (such as chlorination) to effectively remove arsenic from drinking water. The need for pretreatment depends on source water quality.

BARTO REPORT EXCERPTS

SUMMARY

In summary, it is clear that ground water is abundant in the area. Based upon the data reviewed in this investigation, Ron Barto Ground Water Consultant recommends that the maximum ground water extractions should not exceed the average annual replenishable recharge quantities available to the site. Our best estimate of this quantity is about 12,000 to 24,000 acre-feet per year depending upon the actual ground water gradient at the site. Elevations of the reference points at each well and of the adjacent ground should be undertaken by licensed land surveyor to confirm the on-site gradient.

Records of the water levels and the amount of water extracted from these wells should be maintained monthly. A long-term database for this site can be used to refine the ground water management plan for the site. If water levels are not lowered by the recommended maximum ground water extractions over the longterm, then the rate of extractions can be increased without adversely impacting the basin.

The ground water is acceptable quality and generally meets drinking water standards. If agriculture continues to be the chief use of this water, there are no water quality concerns. However, if the water is to be used for domestic consumption, some blending or treatment will be required to meet acceptable levels of fluoride and arsenic.

Commercial grade wells, including a 50-foot sanitary seal, are required by the San Bernardino County, Environmental Health Department, on all wells other than agricultural wells and single residential house wells. It is unclear the depth of the sanitary seal that each of the individual wells at Oasis Ranch has, but all indications are that the deeper 50-foot seal needs to be installed on some if not all of these wells before they could be used for drinking water.

OWNER'S REMARKS

Good Morning, this is Curt Jahnke, sharing with you the uniqueness of Oasis Ranch and more specifically the incredible source of water.

The land itself is quite valuable from the standpoint of growing things because it is all lava ash, and is filled with minerals and nutrients that encourage lush growth.

The land is also valuable for wind power and ideal for solar power. But the huge or the very significant value is in its truly unbelievable source of water. The reason I say unbelievable is because of the uniqueness of its location and the geology underneath the surface and surrounding area. It is located strategically at the mouth at Black Canyon which is the drainage spout or funnel for a huge area to the North of it all the way back to what appears to be even China Lake.

The incredible size of that funnel and the very small spout through which that water flows, or is stationary underground, is amazing. In addition, the area is riddled with faults and maps show a major fault, and there are a number of smaller ones, running Northwest to Southeast immediately South of the ranch, acting like a dam. Which holds back all of the water, or a majority of the water, from moving on South into Harper Lake and surrounding areas.

It is amazing that over the 23 years of alfalfa farming we noticed that Oasis Ranch static water level was always plus or minus 70 feet, even during the 6 years of drought in the late 80's and early 90's. To the South of Oasis Ranch beyond the area of the faults the static water level varied and in many cases was much as 150 feet to 200 feet lower than Oasis Ranch water levels. This substantiates the fact that there is literally a dam holding back the water.

During the 6 years of drought, during the time of the late 80s and early 90s, most wells, if not all wells, in the surrounding area dropped precipitously. At no time during those 6 years was any pump lowered on Oasis Ranch because there was no significant drop in the water table.

The Oasis Ranch was dismissed from the adjudication case in 1996 because of these 3 facts.

Number 1, it was not in the basin that was alleged, even one engineering firm working with the court had reservations about its being included in that basin. The proof was Number 1 the water table on Oasis Ranch was very substantially higher than any of the wells to the south in the alleged basin.

CONTINUED →

Source:

This text was transcribed by Schrader Real Estate and Auction Co., Inc. in January 2013 from an audio recording provided by the Owner for inclusion in this information book.

OWNER'S REMARKS

Number 2 the water quality was markedly different and had no real semblance of being the same source. Some reports indicated that the water at the Oasis Ranch came from the San Bernardino Mountains, which was proven false during the drought when Oasis Ranch wells had a significantly higher water table than most, if not all, wells to the South of the Ranch. It is my understanding that the California Supreme Court determined there were no connections between the water to the South and the water at Oasis Ranch.

The third, the 1st is the water table, the 2nd is the water quality, the 3rd is the proof during the drought period that there was no connection between the water from the South and the water from the North by virtue of the fact that the water levels to the South were very significantly lower.

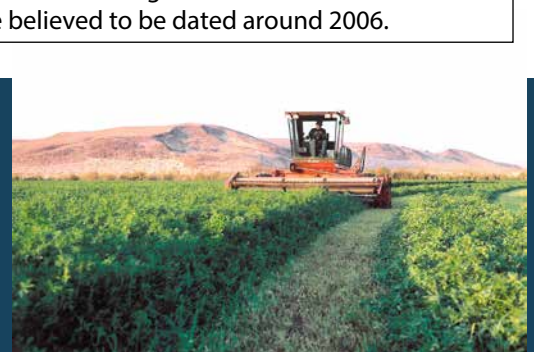
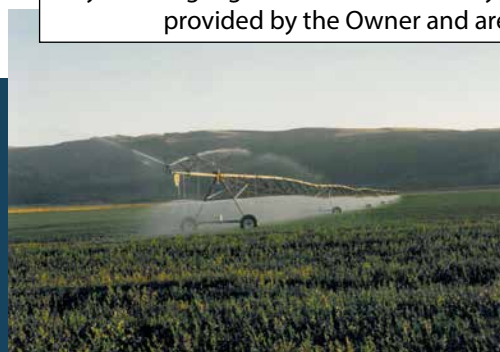
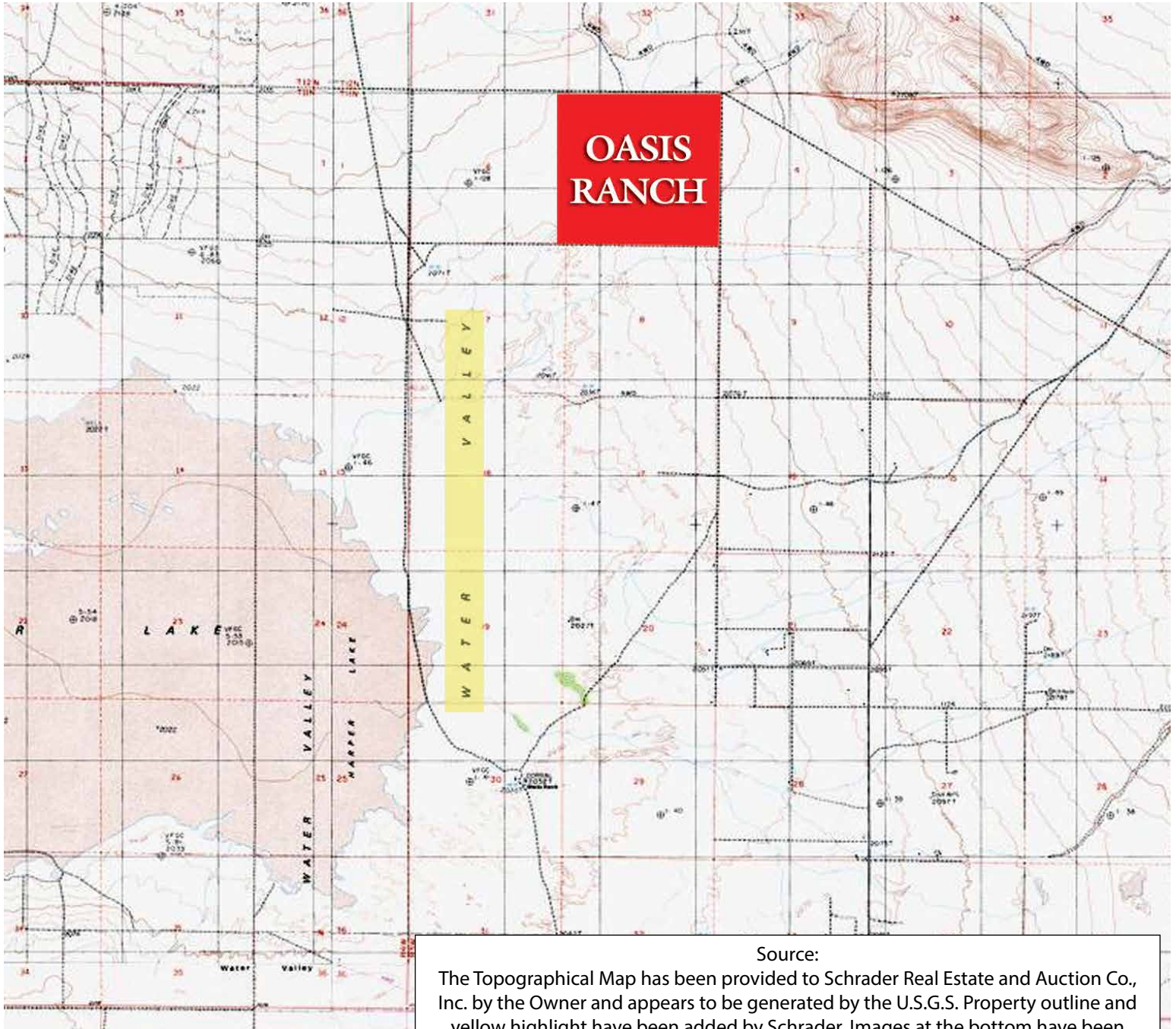
The 4th is that water temperature, in high desert wells, changes significantly from summer to winter. Oasis Ranch water never changes. It is always 64 degrees summer and winter. This indicates to me that the water comes from deep underground and is somehow kept constant at 64 degrees. An exciting exploration was made when it was discovered that there was an old oil well bore hole slightly Northwest of Oasis Ranch, that had been drilled to 3000 feet. The drill log or the e-log shows amazing quantities of water at 200 to 500 feet, then various amounts at various lower levels but a huge amount of water at 2500-3000 feet and the temperature in the bore hole went from 64 degrees when they first hit liquid to 109 degrees at 3000 feet. This sort of substantiates the contention that the water comes from deep down underground and it's almost as though there were a hot plate at the bottom keeping it warm enough and it cools as it comes to the top but it never gets below 64 degrees. Absolutely amazing unique circumstances. And a question is raised in my mind is there another 30,000 feet at 3,000 feet. Amazing.

*Curt Jahnke
Owner of Oasis Ranch
Santa Barbara, California
January 2013*

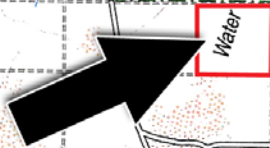
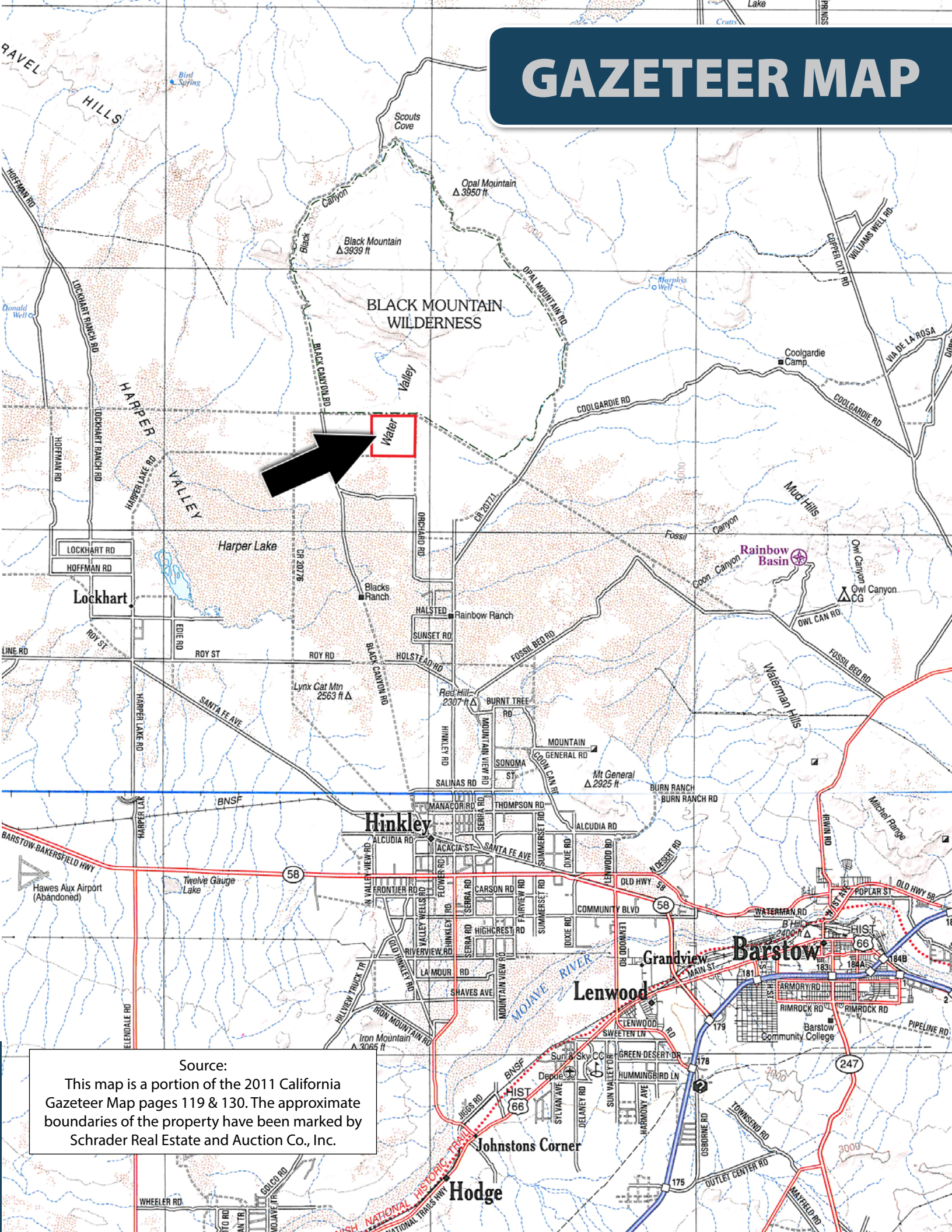
WATER VALLEY

Oasis Ranch, which lies within the historical drainage of Black Canyon, is situated within the more permeable undifferentiated recent alluvium and/or older alluvium.

Historic mapping has indicated an area called Water Valley running across the property.



GAZETEER MAP



BLACK MOUNTAIN WILDERNESS

Hinkley

Lenwood

Barstow

Johnstons Corner

Hodge

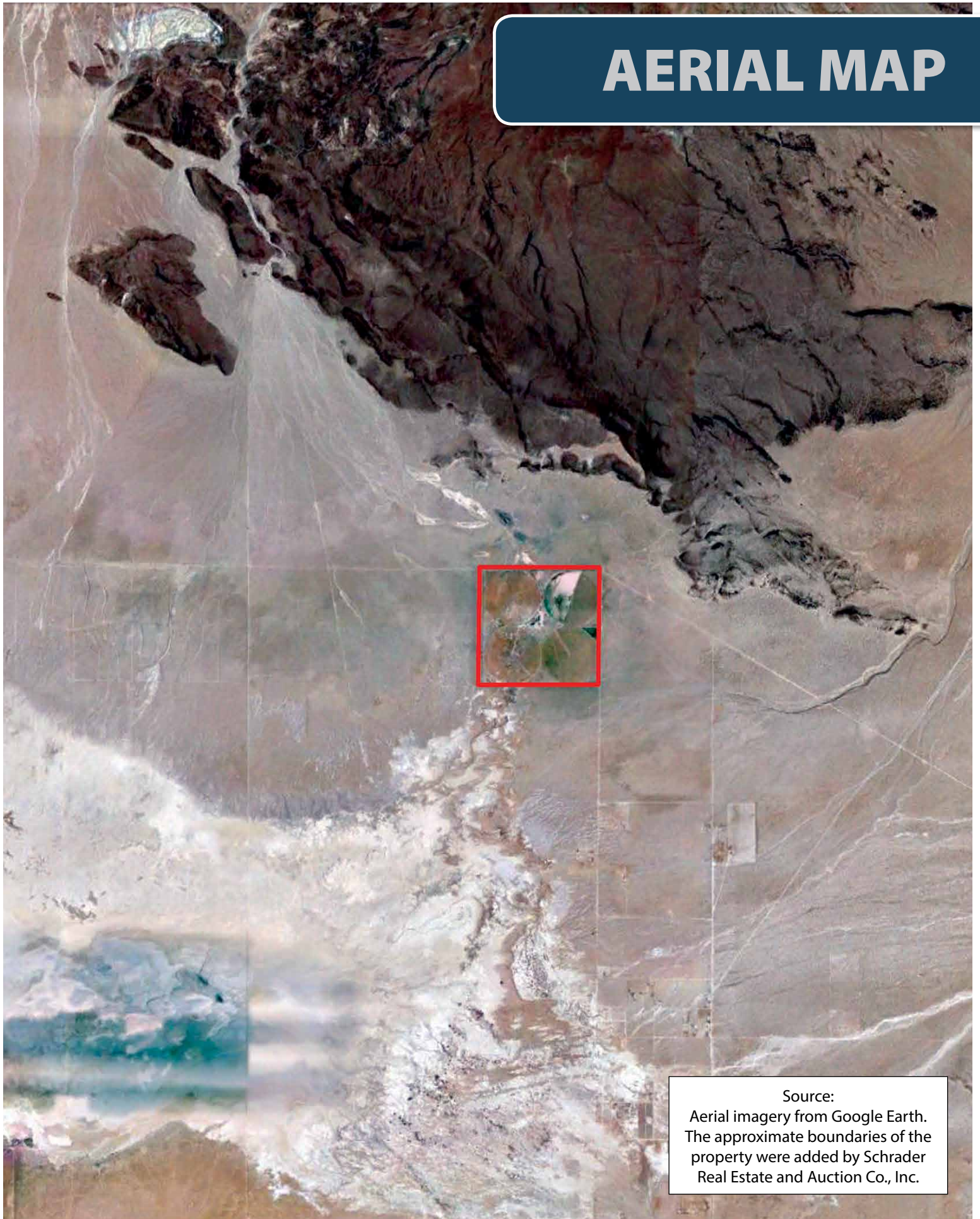
Source:
This map is a portion of the 2011 California Gazetteer Map pages 119 & 130. The approximate boundaries of the property have been marked by Schrader Real Estate and Auction Co., Inc.



Major Population Areas within 100± Miles of Oasis Ranch

Los Angeles.....	9,889,056
Riverside	2,239,620
San Bernardino.....	2,065,377
Orange.....	3,055,745
TOTAL	17,249,798

AERIAL MAP



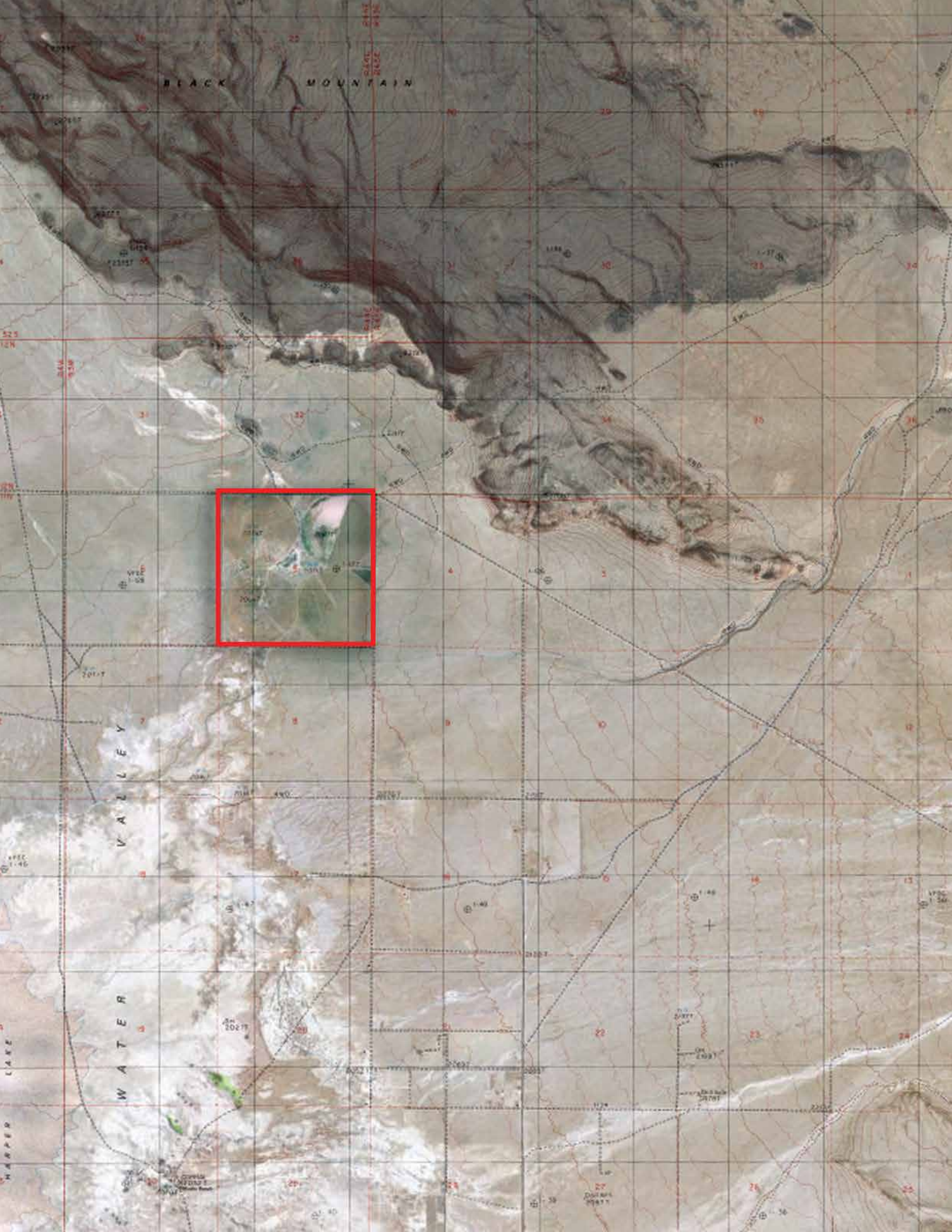
Source:
Aerial imagery from Google Earth.
The approximate boundaries of the
property were added by Schrader
Real Estate and Auction Co., Inc.

TOPOGRAPHIC MAP

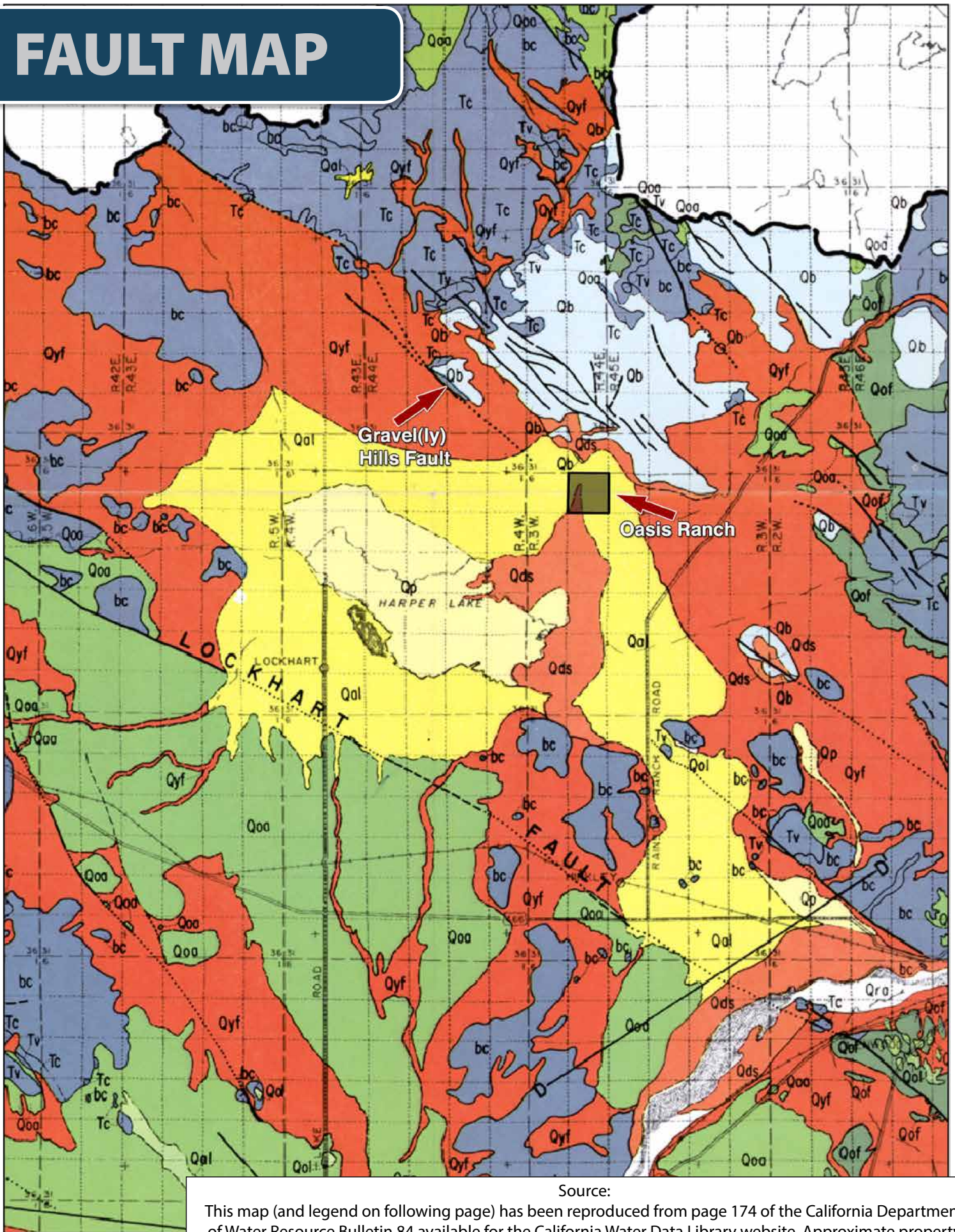
Solar Plant



Source:
Aerial imagery and Topographic overlay from Google Earth. The approximate boundaries of the property and location of the Solar Plant were added by Schrader Real Estate and Auction Co., Inc. The photo of the Solar Plant was from a physical inspection of the site in December 2012.



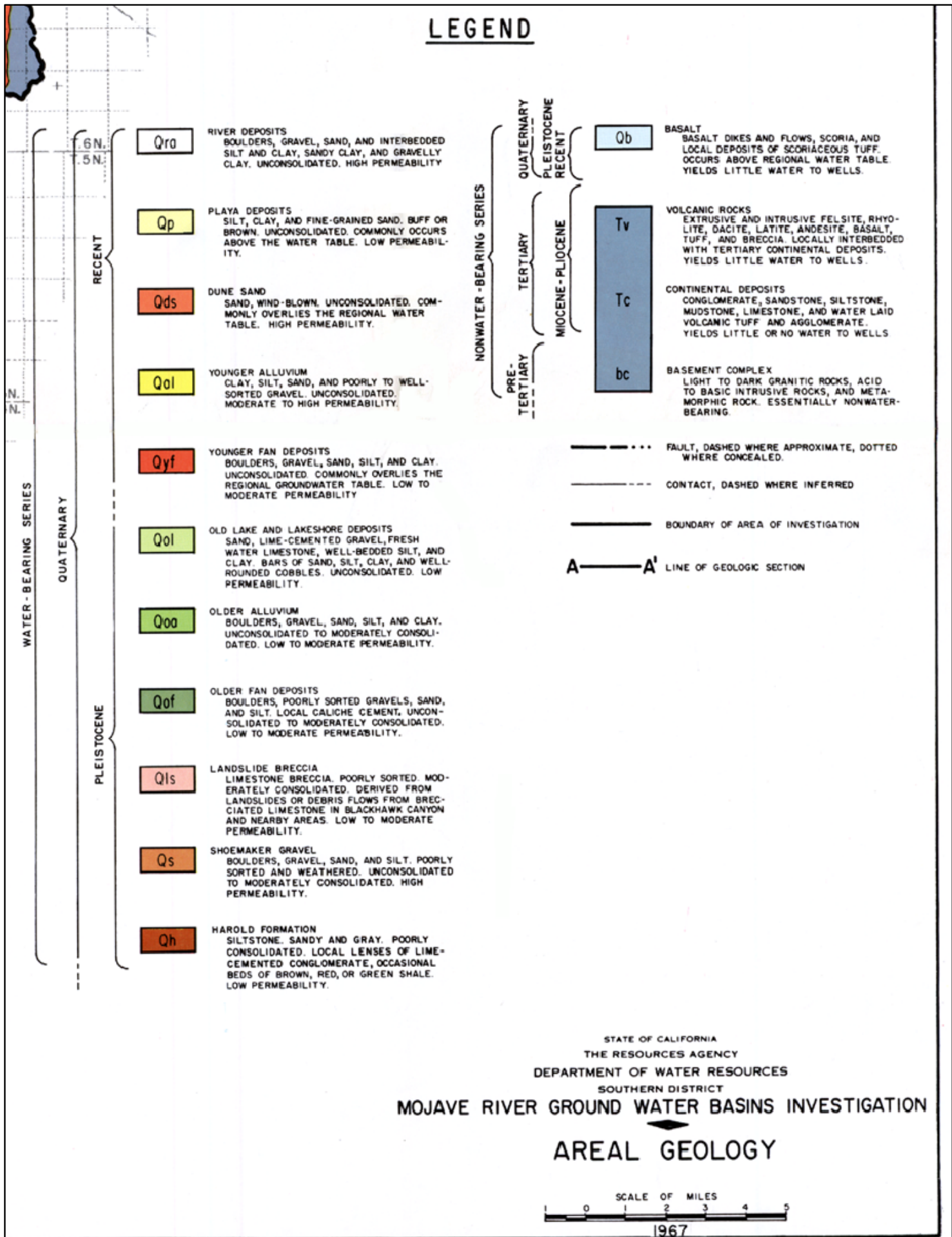
FAULT MAP



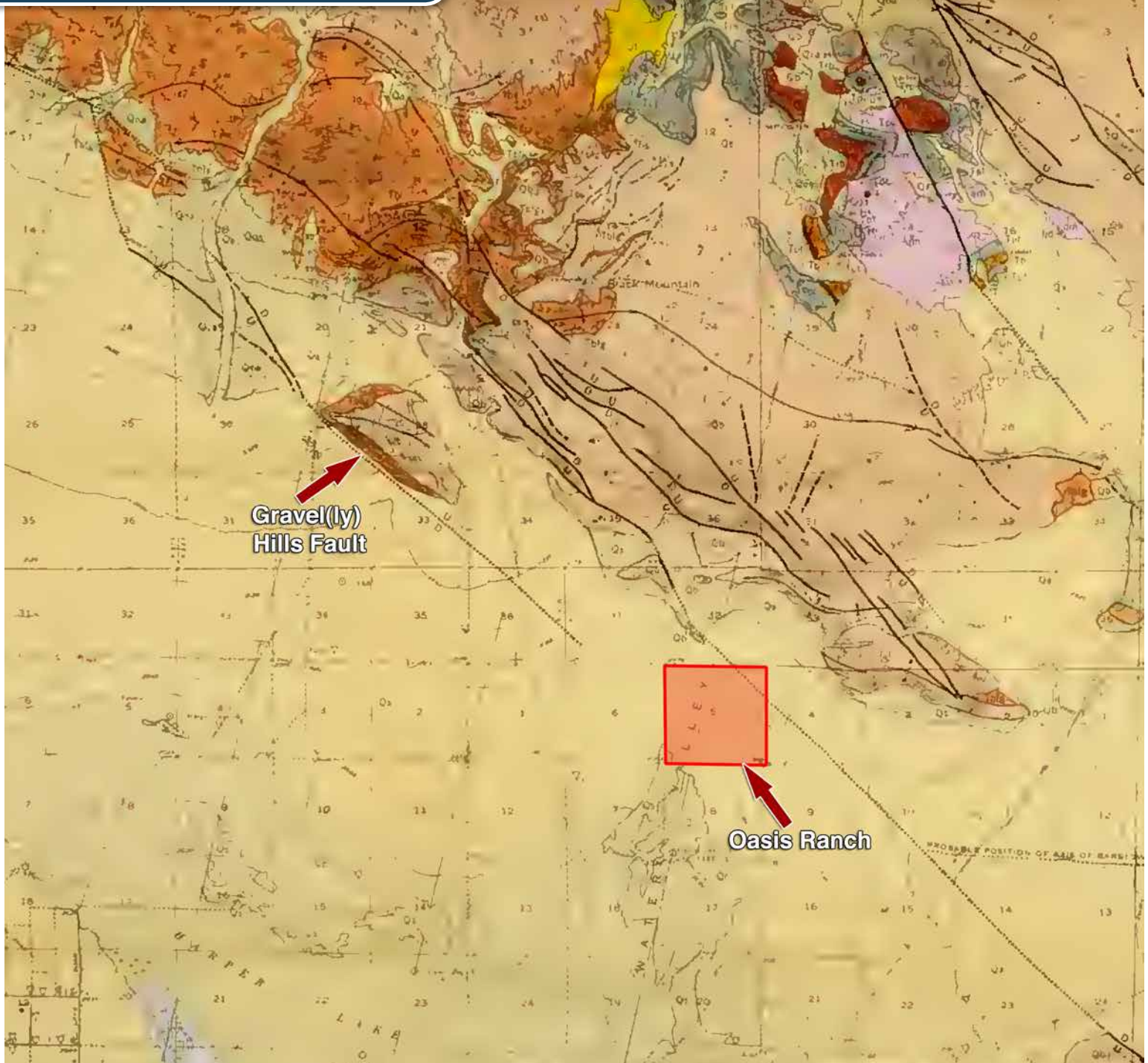
Source:

This map (and legend on following page) has been reproduced from page 174 of the California Department of Water Resource Bulletin 84 available for the California Water Data Library website. Approximate property boundaries and fault label were added by Schrader Real Estate and Auction Co., Inc. Fault label is from data in a separate map.

LEGEND



FAULT MAP



Gravel(l)y
Hills Fault

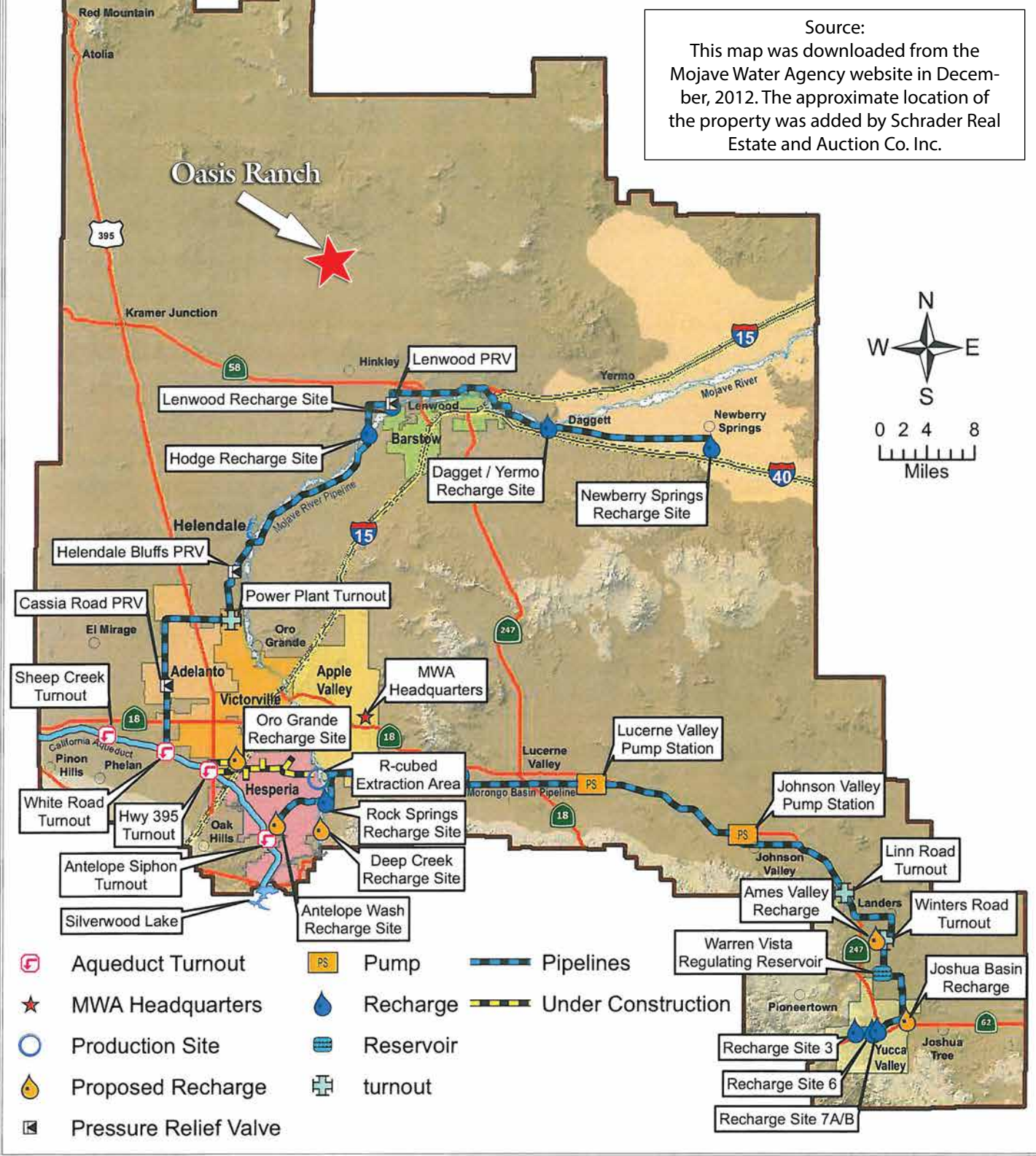
Oasis Ranch

This portion of the Mojave Desert is crosscut by a series of northwest-trending faults, including the Helendale, Camp Rock-Harper Lake, and Calico-Newberry faults. Geologic features, along with roads and fences that have been offset by historic earthquakes show that these faults characteristically generate rightlateral strike-slip displacements consistent with those of the nearby, more active San Andreas Fault Zone. Some of the faults also show evidence of vertical displacement. The nearby Lockhart and Mt. General faults cross the valley southwest of the Project Site and appear to act as a barrier to ground water flow. The Gravel Hills fault and the northwestern extension of the Camp Rock-Harper Lake fault are projected to cut across the valley near the Oasis Ranch site.

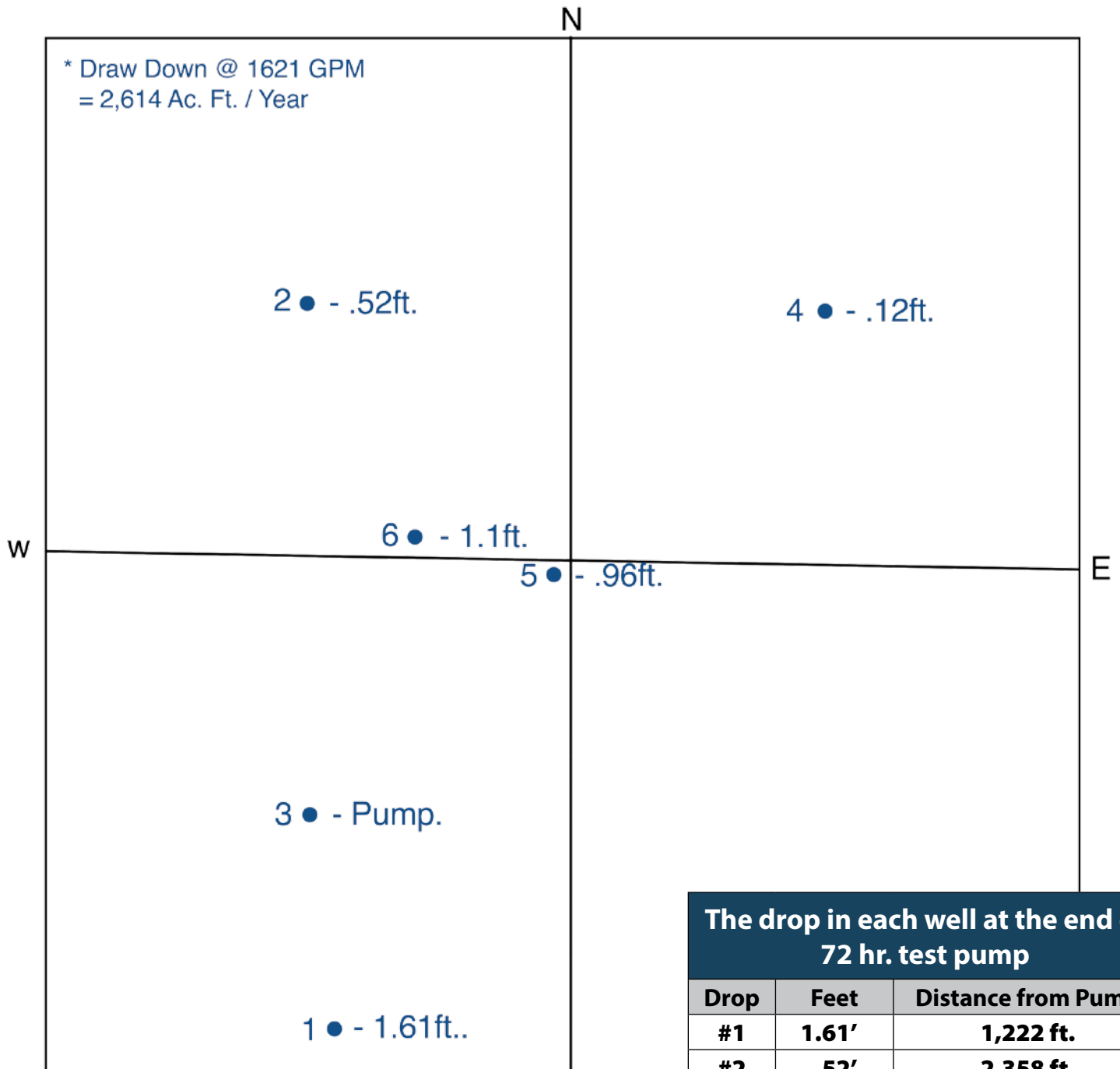
Source: This is a cropped area from a map reproduced from page 72 of "Geology of the Freeman Peak and Opal Mountain Quadrangles, California" by T.W. Wilson published as Bulletin 188 by the California Division of Mines and Geology and available as a download from archive.org. Approximate property boundaries and fault label were added by Schrader Real Estate and Auction Co., Inc. Fault label has been included for reference as original label is outside the cropped area. The text is an excerpt from a Hydrogeologic Evaluation prepared by Ron Barto Water Consultant in 2011, provided to Schrader Real Estate and Auction Co., Inc. by the Owner.

Mojave Water Agency Water Delivery Facilities

Source:
This map was downloaded from the Mojave Water Agency website in December, 2012. The approximate location of the property was added by Schrader Real Estate and Auction Co. Inc.



TEST PUMP WELL LOCATION & DRAW DOWN



The drop in each well at the end of 72 hr. test pump

Drop	Feet	Distance from Pump
#1	1.61'	1,222 ft.
#2	.52'	2,358 ft.
#3	Pump	1 ft.
#4	.12'	3,732 ft.
#5	.96'	1,824 ft.
#6	1.1'	1,386 ft.

Source:

This chart and table have been created using well test pump data from a Hydrogeologic Evaluation prepared by Ron Barto Ground Water Consultant in 2011, provided to Schrader Real Estate and Auction Co., Inc. by the Owner. Raw pump data is provided in Appendix B of this information booklet.

Pumping rate - 1621 GPM

PAST CROPPING INFORMATION



OASIS RANCH -

Oasis Ranch is an oasis of alfalfa on the desert. The ranch is 640 acres in size and operates at an elevation of over 2,000 feet above sea level. Located on the ranch is a 2,500 ton hay barn, a machine shop, and three residences for farm technicians.

ALFALFA -

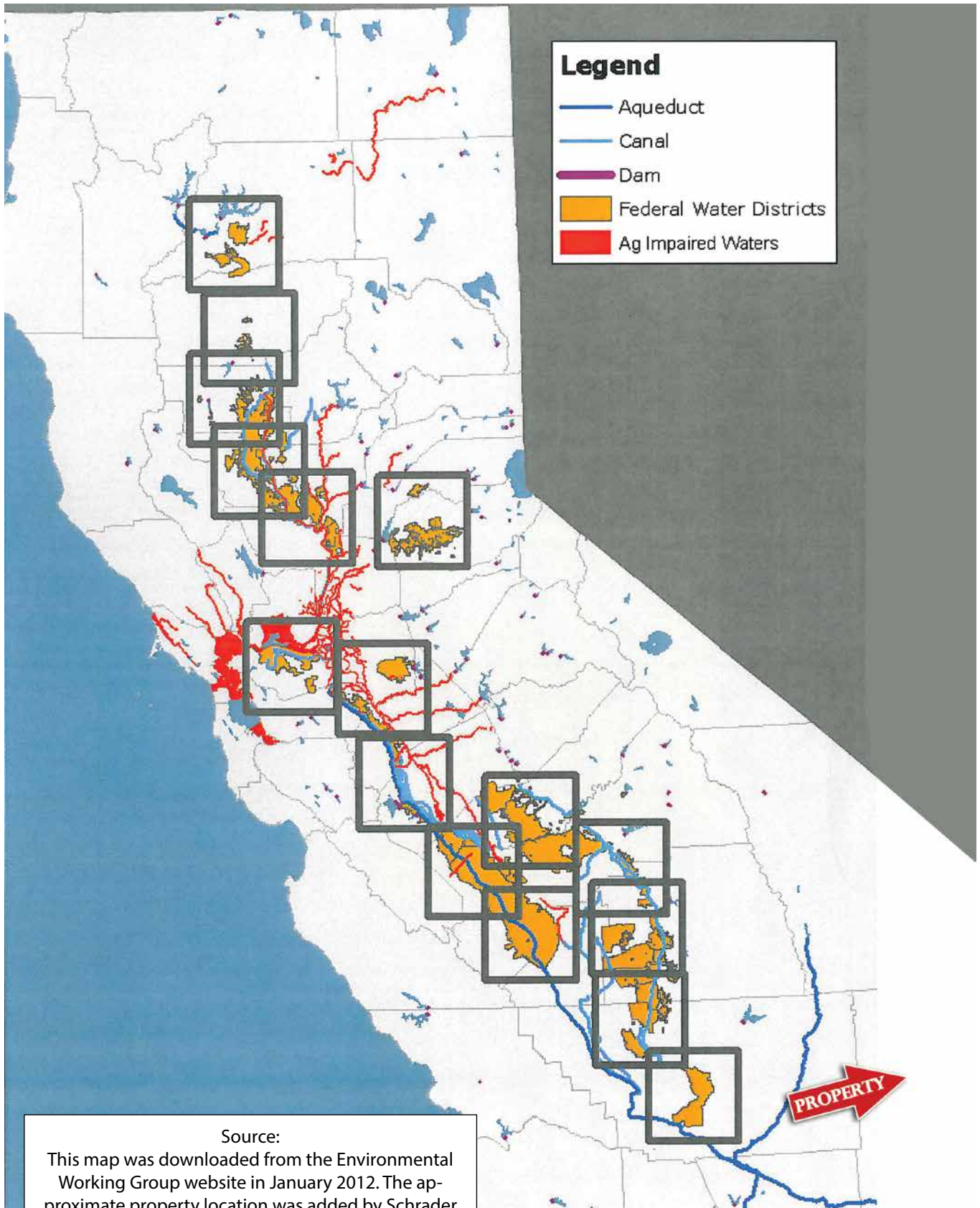
Oasis Ranch grows high quality alfalfa. The crop is green, leafy, and clean. Oasis Ranch is situated at the base of Black Mountain. This location provides a unique climate of less wind and excellent dew conditions even in mid-summer. The abundant supply of water keeps growth lush, green, and soft.



Source:

Text and photography are from an advertising piece created and provided by the Owner to Schrader Real Estate and Auction Co., Inc. Photographs are believed to be from 2006 or earlier.

WATER TRANSPORTATION



Source:
This map was downloaded from the Environmental Working Group website in January 2012. The approximate property location was added by Schrader Real Estate and Auction Co., Inc.

AREA MAP



Source:
Aerial imagery from Google Earth.
The approximate boundaries of the
property were added by Schrader
Real Estate and Auction Co., Inc.

PROPERTY PHOTOS



PROPERTY PHOTOS



View looking south towards property showing watershed area north of Oasis Ranch.



Looking northeast toward Oasis Ranch from Solar Plants.

PROPERTY PHOTOS



Area North of Black Mountain



Photo indicating flow of water near Oasis Ranch

PROPERTY PHOTOS



Channel on the east side of Black Mountain showing flow of water toward Oasis Ranch



West side of Black Mountain showing flow of water through Black Canyon toward Oasis Ranch

PROPERTY PHOTOS



PROPERTY PHOTOS



PROPERTY PHOTOS



PROPERTY PHOTOS



SOLAR PLANT



CALIFORNIA AQUEDUCT



RIGHT OF ENTRY AGREEMENT

RIGHT OF ENTRY AND ACCESS AGREEMENT

THIS RIGHT OF ENTRY AND ACCESS AGREEMENT (herein called this "Agreement") is made and entered into as of _____, 2013, by the Ace Exploration and Water Drilling Company ("Licensor"), and _____ (the "Licensee")

WITNESSETH:

WHEREAS, Licensor is the owner of the real property in San Bernardino County, California described as follows (herein called the "Property"):

SECTION 5, TOWNSHIP 11 NORTH, RANGE 3 WEST, SAN BERNARDINO BASE AND MERIDIAN;

WHEREAS, concurrently with the execution of this Agreement, Licensee is interested in making an effort to purchase the Property at auction;

WHEREAS, Licensee needs the right of entry upon and access to the Property for the purpose of undertaking inspections and other due diligence activities (not including invasive activities such as drilling without the prior written consent of Licensor) (herein called the "Due Diligence Activities") required in connection with the potential acquisition by Licensee of the Property;

WHEREAS, Licensor has agreed to grant to Licensee, and Licensee has agreed to accept from Licensor, a non-exclusive license to enter upon the Property to perform the Due Diligence Activities in accordance with the terms and provisions of this Agreement;

WHEREAS, Licensor and Licensee desire to execute and enter into this Agreement for the purpose of setting forth their agreement with respect to the Due Diligence Activities and Licensee's entry upon the Property.

NOW, THEREFORE, for and in consideration of the foregoing premises, the mutual covenants and agreements contained herein, and other good and valuable consideration, the receipt and sufficiency of which are hereby acknowledged, Licensor and Licensee do hereby covenant and agree as follows:

1. Access by Licensee. Subject to Licensee's compliance with the terms and provisions of this Agreement, Licensee and Licensee's employees, agents and consultants designated in writing by Licensee (herein collectively called "Licensee's Designees") shall have the right to enter upon the Property for the purpose of conducting the Due Diligence Activities, until _____, 2013.

Licensee expressly agrees as follows: (i) any activities by or on behalf of Licensee, including, without limitation, the entry by Licensee or Licensee's Designees onto the Property in connection with the Due Diligence Activities shall not damage the Property in any manner whatsoever; (ii) in the event the Property is altered or disturbed in any manner in connection with the Due Diligence Activities, Licensee shall immediately return the Property to the condition existing prior to the Due Diligence Activities, and (iii) Licensee shall indemnify, defend and hold Licensor harmless from and against any and all claims, liabilities, damages, losses, costs and expenses of any kind or nature whatsoever (including, without limitation, attorneys' fees and expenses and court costs) suffered, incurred or sustained by Licensor as a result of, by reason of, or in connection with the Due Diligence Activities or the entry by Licensee or Licensee's Designees onto the Property, except to the extent they

RIGHT OF ENTRY AGREEMENT

are caused by the negligence or willful misconduct of the Licensee, or its agents, contractors or employees.

2. Lien Waivers. Upon receipt of a written request from Licensor, Licensee will provide Licensor with lien waivers following completion of the Due Diligence Activities from each and every contractor, materialman, engineer, architect and surveyor who might have lien rights, in form and substance reasonably satisfactory to Licensor and its counsel. To the extent permitted by applicable law, Licensee hereby indemnifies Licensor from and against any claims or demands for payment, or any liens or lien claims made against Licensor or the Property as a result of the Due Diligence Activities.

3. Insurance. Licensee shall, and shall cause all of Licensee’s Designees performing the Due Diligence Activities to, procure or maintain a policy of commercial general liability insurance issued by an insurer reasonably satisfactory to Licensor covering each of the Due Diligence Activities with a single limit of liability (per occurrence and aggregate) of not less than \$1,000,000.00, and to deliver to Licensor a certificate of insurance evidencing that such insurance is in force and effect, and evidencing that Licensor has been named as an additional insured thereunder with respect to the Due Diligence Activities. Such insurance shall be maintained in force throughout the term of this Agreement. If Licensee’s Designees used for Due Diligence Activities are unable to meet these insurance requirements on their own, Licensee may provide such coverage on their behalf.

4. Successors. To the extent any rights or obligations under this Agreement remain in effect, this Agreement shall be binding upon and enforceable against, and shall inure to the benefit of, the parties hereto and their respective heirs, legal representatives, successors and permitted assigns.

5. Limitations. Licensor does not hereby convey to Licensee any right, title or interest in or to the Property, but merely grants the specific and limited contractual rights set forth herein.

6. Assignment. This Agreement may not be assigned by Licensee, in whole or in part, without the prior express written consent of the Agency in its sole and absolute discretion.

7. Governing Law. This Agreement shall be construed, enforced and interpreted in accordance with the laws of the State of California.

8. Counterparts. This Agreement may be executed in several counterparts, each of which shall be deemed an original, and all of such counterparts together shall constitute one and the same instrument.

IN WITNESS WHEREOF, Licensor and Licensee have caused this Agreement to be executed and sealed, on the day and year first written above.

LICENSEE:

By: _____

Print Name: _____

Title: _____

LICENSOR:

Ace Exploration and Water Drilling Company

By: _____

Print Name: Curtis Jahnke

Title: President

Bidder # _____

BIDDER PRE-REGISTRATION FORM

640 ACRES • BARSTOW, CALIFORNIA

THURSDAY, FEBRUARY 28, 2013

This form must be received at Schrader Real Estate and Auction Company, Inc.,
P.O. Box 508, Columbia City, IN, 46725,
Fax # 260-244-4431, no later than Thursday, February 21, 2013.

BIDDER INFORMATION

Name _____

Address _____

City/State/Zip _____

Telephone: (Res) _____ (Office) _____

My Interest is in Property or Properties # _____

BANKING INFORMATION

Check to be drawn on: (Bank Name) _____

City, State, Zip: _____

Contact: _____ Phone No: _____

HOW DID YOU HEAR ABOUT THIS AUCTION?

Brochure Newspaper Signs Internet Radio TV Friend

Other _____

WOULD YOU LIKE TO BE NOTIFIED OF FUTURE AUCTIONS?

Regular Mail E-Mail E-Mail address: _____

Tillable Pasture Ranch Timber Recreational Building Sites

What states are you interested in?

Note: If you will be bidding for a partnership, corporation or other entity, you must bring documentation with you to the auction which authorizes you to bid and sign a Purchase Agreement on behalf of that entity.

I hereby agree to comply with terms of this sale including, but not limited to, paying all applicable buyer's premiums, and signing and performing in accordance with the contract if I am the successful bidder. Schrader Real Estate and Auction Company, Inc. represents the Seller in this transaction.

Signature: _____ Date: _____

Online Auction Bidder Registration
640± Acres • Barstow, California
Thursday, February 28, 2013

This registration form is for the auction listed above only. The person signing this form is personally responsible for any bids placed on the auction site, whether bidding on behalf of their personal account or on behalf of a corporation or other third party. If you are bidding on behalf of a third party, you are responsible for obtaining the necessary documentation authorizing you to bid on behalf of the third party. Schrader Real Estate and Auction Co., Inc. will look to the herein registered bidder for performance on any bid placed on this auction if you are the successful high bidder.

As the registered bidder, I hereby agree to the following statements:

1. My name and physical address is as follows:

My phone number is: _____

2. I have received the Real Estate Bidder's Package for the auction being held on Thursday, February 28, 2013 at 1:00 PM.
3. I have read the information contained in the Real Estate Bidder's Package as mailed to me or by reading the documents on the website (www.schraderauction.com) and understand what I have read.
4. I hereby agree to comply with all terms of this sale, including paying all applicable buyer's premiums, and signing and performing in accordance with the Real Estate Purchase Agreement if I am the successful bidder.
5. I understand that Schrader Real Estate and Auction Co., Inc. represent the Seller in this transaction.
6. I am placing a deposit with Schrader Real Estate and Auction Co., Inc. Escrow in the amount of \$_____. I understand that the maximum bid or combination of bids I place may not exceed an amount equal to ten times the amount of my deposit. My deposit is being conveyed herewith in the form of a cashier's check payable to Schrader Real Estate and Auction, Co., Inc. Escrow or via wire transfer to the escrow account of Schrader Real Estate and Auction, Co., Inc. per the instructions enclosed with the Bidder's Package. I understand that my deposit money will be returned in full if I am not



DVD with interviews by the Owner, Attorney James Markman, and Robert Beeby available upon request by calling the Auction Company at 800-451-2709

APPENDIX A

ON-SITE WELL LOGS

Source:

Appendix taken directly from a Hydrogeologic Evaluation prepared by Ron Barto Ground Water Consultant in 2011, provided to Schrader Real Estate and Auction Co., Inc. by the Owner.

172/12
Copy

STATE OF CALIFORNIA
THE RESOURCES AGENCY
DEPARTMENT OF WATER RESOURCES
WATER WELL DRILLERS REPORT

Do not fill in
No. 127827

File of Intent No. 101428
Permit No. or Date 09177902

State Well No. _____
Other Well No. _____

OWNER: Name C.R. Jahnke
4900 Cathedral Road
Santa Barbara, California
Zip _____
LOCATION OF WELL (See instructions):
San Bernardino (See instructions):
Owner's Well Number _____
Address if different from above _____
City _____ Range _____ Section 5
County _____
Minkley, California

(12) WELL LOG: Total depth _____ ft. Depth of completed well 355 ft.

from ft.	to ft.	Formation (Describe by color, character, size or material)
0	2	Top soil, clay
2	37	Sand and gravel w/ some rocks
37	40	90% brown clay, 5% rocks, 5% sand
40	46	Sand and gravel, some pea size
46	68	80% brown clay, some rocks
		18% sand and gravel
68	78	45% brown clay, sand and gravel
78	81	Sand and gravel
81	91	60% brown clay, sand and gravel
91	120	Sand and gravel
120	130	55% brown clay, sand and gravel
130	140	90% brown clay, sand and gravel
140	144	90% clay
144	162	20% clay, sand and gravel
162	168	Sand and gravel
168	180	50% clay and gravel
180	190	15% clay and gravel
190	193	25% clay and gravel
193	200	10% clay
200	210	15% clay and gravel
210	220	15% clay and gravel
220	230	10% clay and gravel
230	240	very little clay and gravel
240	253	Sand
253	280	Sand and gravel, very little clay
280	285	10% clay and sand
285	295	Very little clay and sand
295	319	Sand and gravel
319	318	Large pea gravel and sand
318	321	Large pea gravel and sand
321	328	35% clay and sand
328	333	Volcanic tuff, gravel and sand
		little clay
333	345	Small pea gravel and sand
345	355	Volcanic rock

WELL #1

(3) TYPE OF WORK:
New Well Deepening
Reconstruction
Reconditioning
Horizontal Well
Destruction (Describe destruction materials and procedures in Item 12)
(4) PROPOSED USE:
Domestic
Irrigation
Industrial
Test Well
Stock
Municipal
Other

WELL LOCATION SKETCH

EQUIPMENT:
 Reverse
 Air
 Bucket
(8) GRAVEL PACK:
Yes No Size _____
Diameter of bore 12" _____
Packed from 0 to 355 ft.
CASING INSTALLED:
 Plastic Concrete
(8) PERFORATIONS:
Type of perforation or size of screen _____

WELL SEAL:
Surface sanitary seal provided? Yes No If yes, to depth _____ ft.
Casing sealed against pollution? Yes No Interval _____ ft.
Type of sealing _____

WATER LEVELS:
Depth of first water, if known _____ ft.
Static level after well completion _____ ft.

WELL TESTS:
Well test made? Yes No If yes, by whom? _____
Type of test _____
Flow rate at start of test _____ ft.
Flow rate _____ gal/min after _____ hours
Water temperature _____
Well analysis made? Yes No If yes, by whom? _____
Electric log made? Yes No If yes, attach copy to this report

Work started 9/24 19 79 Completed 10/4/ 19 79
WELL DRILLER'S STATEMENT:
This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.
Signed: Wayne Landrith
(Well Driller)
NAME: Howard Pump, Inc
(Person, firm, or corporation) (Typed or printed)
Address: 28753 Hwy 58
City: Barstow, California Zip 92311
License No. 281814 Date of this report 10/9/79

HOWARD PUMP, INC.

PUMP TEST DATA FIELD REPORT

NAME _____ WELL DIAMETER _____ WELL DEPTH _____
 ADDRESS Santa Barbara, California STATIC WATER LEVEL 40'
 LOCATION OF WELL _____ PUMP SETTING 300' AIR LINE _____
 DATE OF DRILLING _____
 WELL NO. Post Hole TEST _____ SHEET _____ OF _____

DATE/TIME	SPECIFIC YIELD ()	DISCHARGE RATE ()	DRAW DOWN ()	REMARKS
10:00	14.20	200	60	
10:05	14.20	200	70	
10:10	13.04	300	65	Increased well to 300 GPM, water became milky
10:15	13.04	300	63	for 1 min.
10:20	13.75	400	60	Increased production to 400 GPM, water
10:25	15.75	400	60	remained dirty 1 min. (changed orifice)
10:30	13.51	500	70	Increased production to 500 GPM, water
10:35				pumping very dirty
10:40	13.51	500	70	
10:45	13.04	500	65	Increased production to 600 GPM, water milky
10:50	13.04	600	66	
10:55	13.33	800	100	Increased to 800 GPM to find if I can pump
11:00				well off. Water pumping dirty and purping;
11:05				no air.
11:10	13.33	600	110	Water slightly dirty, no air. (Sealhead
11:15				leaking oil at this spot)
11:20	11.75	200	50	Decreased gallonage and started at 200 GPM
11:25				to work on upper strata. Water did not dirty
11:30	11.75	200	57	up after surging 5 times (changed orifice)
11:35	11.75	200	57	surged 5 times and then resumed at 200 GPM
11:40	11.76	200	57	water took 1 min. to clear up after surging
11:45	11.76	200	57	surged well and resumed at 200 GPM, no dirty
11:50				water at this time
11:55	12.30	200	50	Pumping level came up 1 foot
12:00		200	50	surged 5 times, then resumed pumping at 200 GPM
12:05		200	50	Water remains clear
12:10		400		surged 5 times, then increased well to 400 GPM
12:15				(Changed orifice to 6")
12:20	14.20	400	60	Water did not become dirty
12:25		400		surged 5 times, then resumed at 400 GPM
12:30				water remains clear
12:35	13.33	400	70	Pump level dropped 2 ft from 11:40 reading.

HOWARD PUMP, INC.

PUMP TEST DATA
FIELD REPORT

NAME J. ... WELL DIAMETER ... WELL DEPTH 325'
 ADDRESS Santa Barbara, California STATIC WATER LEVEL 40'
 LOCATION OF WELL ... PUMP SETTING 300' AIR LINE ...
 WELL NO. Test Well DATE OF DRILLING ...
 TEST NO. ... SHEET 2 OF ...

DATE/TIME	SPECIFIC YIELD	DISCHARGE RATE	DRAW DOWN	REMARKS
11:00 am		400		...
11:10	14.8	400	60	...
11:15		400		...
11:20	14.8	400	60	...
11:30		600		...
11:40	14.28	600	60	...
11:45		600		...
11:50	13.63	600	60	...
1:00 pm		600		...
1:10	13.63	600	60	...
1:15		600		...
1:20	13.07	600	60	...
1:30		600		...
1:40	13.11	600	101	...
1:45		600		...
1:55	13.11	600	101	...
2:00		600		...
2:10	13.11	600	101	...
2:15		600		...
2:20	12.90	600	102	...
2:30	12.90	600	102	...
2:45	12.5	600	104	...
3:00	12.5	600	104	...
3:15	12.51	600	105	...

STATE
er's Copy

STATE OF CALIFORNIA

THE RESOURCES AGENCY

DEPARTMENT OF WATER RESOURCES
WATER WELL DRILLERS REPORT

Do not fill in

No. 127820

101428

of Intent No. 09177902

Permit No. or Date

#2

State Well No.

Other Well No.

OWNER: Name C.R. Janke
4900 Cathedral Road
Santa Barbara, California Zip _____
LOCATION OF WELL (See instructions):
San Bernardino Owner's Well Number _____

Address if different from above:
11N Range 3W Section 5
from cities, roads, railroads, fences, etc.
parcel #489-161-11

(12) WELL LOG: Total depth _____ ft. Depth of completed well 207 ft.

from ft.	to ft.	Formation (Describe by color, character, size or material)
0	20	6% sand and gravel w/ brown clay
20	30	Sand and gravel, 3% greenish brown clay
30	50	6% greenish clay w/ sand & gravel
50	60	Sand & gravel w/ touch of clay
60	70	4% brownish green clay w/ sand and gravel
70	90	Sand and gravel w/ touch of clay
90	120	Green clay w/ very little sand

WELL #2

FIELD

- (3) TYPE OF WORK:
- New Well Deepening
 - Reconstruction
 - Reconditioning
 - Horizontal Well
 - Destruction (Describe destruction materials and procedures in Item 12)

- (4) PROPOSED USE:
- Domestic
 - Irrigation
 - Industrial
 - Test Well
 - Stock
 - Municipal
 - Other

WELL LOCATION SKETCH

PAVEMENT:

- Reverse
- Air
- Bucket

(6) GRAVEL PACK:

Yes No Size _____
Diameter of bore _____
Packed from _____ to _____ ft.

(8) PERFORATIONS:

Plastic Concrete Type of perforation or size of screen _____

To ft.	Dia. in.	Gage or Wall	From ft.	To ft.	Slot size

WELL SEAL:

Sanitary seal provided? Yes No If yes, to depth _____ ft.
Sealed against pollution? Yes No Interval _____ ft.
Sealing _____

WATER LEVELS:

Static water, if known _____ ft.
Level after well completion _____ ft.

WELL TESTS:

Test made? Yes No If yes, by whom? _____
Pump Bailor Air lift
After at start of test _____ ft. At end of test _____ ft.
_____ gal/min after _____ hours Water temperature _____
Analysis made? Yes No If yes, by whom? _____
Log made? Yes No If yes, attach copy to this report

Work started _____ 19____ Completed _____ 19____

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

SIGNED: Wayne Landrith

NAME: Howard Pump, Inc (Well Driller)

(Person, firm, or corporation) (Typed or printed)

Address: 28753 Hwy 58

City: Barstow, California Zip: 92311

License No. 281814 Date of this report: 10/22/79

HOWARD PUMP, INC.
PUMP TEST DATA
FIELD REPORT

NAME C. W. Jahnke WELL DIAMETER 14" WELL DEPTH 206
 ADDRESS _____ STATIC WATER LEVEL 58
 LOCATION OF WELL Winkley Area PUMP SETTING 100 AIR LINE 160
 DATE OF DRILLING October 1979
 WELL NO. _____ TEST Development SHEET 1 OF 1

DATE/TIME	SPECIFIC YIELD per ft	DISCHARGE RATE gpm)	DRAW DOWN (ft)	REMARKS
10/22/79				
10:25 am			58	Checked static water level
10:30	17.11	300	75	Started pumping at discharge rate of 300 GPM Pumping dirty water
10:40	21.42	300	72	Water still pumping dirty, had to adjust throttle to compensate for pumping level rising
10:50	25.0	300	70	Readjust throttle again, still pumping dirty
11:00	25.0	300	70	Pumping level stabilized, still pumping dirty
11:15	25.0	300	70	Pumping level remains stabilized, still pumping dirty
11:25	25.0	300	70	Water is pumping clear
11:30	25.0	300	70	Surged well 3 times and began pumping again at 300 gpm
11:45	25.0	300	70	Still pumping dirty
11:55	25.0	300	70	Almost clear water
12:00 noon		300		Surged well 4 times and resumed pumping at 300 gpm
12:10	20.0	300	73	Water pumping clear with very little if any sand
12:15	20.0	300	73	Surged well 4 times, then resumed at 300 GPM
12:25	20.0	300	73	Water clear
12:30		500		Surged well 3 times, then increased discharge rate to 500 GPM
12:40	20.0	500	83	Water still pumping dirty
12:45		500	83	Water pumping clear, surged 4 times then proceeded at 500 GPM discharge rate
12:55	20.0	500	83	Water remained dirty 4 min.
1:00 pm		500	83	Surged well 4 times then remained at 500 GPM
1:10	20.0	500	83	Water remained dirty 3 min.
1:15		500	83	Surged 4 times, then resumed at discharge rate of 500 GPM
1:25	20.0	500	83	Water remained dirty 4 min.
1:30		500		Surged well 4 times then increased well to 800 GPM
1:40	13.62	800	110	Water clear in 4 min.
1:45		800		Surged well 4 times then resumed a discharge rate of 800 GPM

HOWARD PUMP, INC.

PUMP TEST DATA

FIELD REPORT

NAME Johnke WELL DIAMETER 14" WELL DEPTH 206'
 ADDRESS _____ STATIC WATER LEVEL 48
 LOCATION OF WELL Winkley Area PUMP SETTING 100 AIR LINE 160
 DATE OF DRILLING October 1977
 WELL NO. _____ TEST Development SHEET 2 OF _____

DATE TIME	SPECIFIC YIELD (per ft)	DISCHARGE RATE (GPM)	DRAW DOWN (ft)	REMARKS
10/22/77				
1:55 pm	13.62	800	110	Water remained dirty 3 min.
2:00		800		Surged well then resumed 800 GPM
2:10	13.62	800	110	Water remained dirty for 4 min.
2:15		500		Surged well 4 times then resumed a discharge rate of 800 GPM
2:25	13.62	500	110	Water remained dirty for 2 min.
2:30		1000		Surged well 3 times then increased discharge rate to 1000 GPM
2:35	12.19	1000	140	Water dirty, adjust throttle to keep up with dropping pumping level
2:40	11.76	1000	143	Adjust throttle to compensate for pumping level dropping
2:45	11.76	1000	143	Adjust throttle to compensate for pumping level dropping
2:50	11.76	1000	143	Water still dirty
2:55	11.76	1000	143	Water still dirty
3:00	11.49	1000	145	Pumping level seems to be dropping, water has become clear
3:10	10.86	1000	150	Water clear, pumping level continues to drop
3:20	10.75	1000	151	Pumping level continues to drop
3:25	10.63	1000	152	Pumping level continues to drop
3:30		300	xxx	Surged, then decreased rate to 300 GPM
3:40	12.5	300	82	Didn't pump any dirty water
3:45		500		Surged well 5 times, then increased discharge rate to 500 GPM
3:55	13.88	500	94	Well pumped no dirty water
4:00		800		Surged well 4 times then increased to 800 GPM
4:10	15.78	800	110	Pumped a slight amount of dirty water
4:15		1000		Surged well then increased to 1000 GPM
4:25	12.19	1000	140	Pumped no dirty water
4:35	11.90	1000	142	Continued pumping at 1000 GPM to check for pumping level drop
4:44	11.62	1000	144	
4:45		500		Decreased to 500 GPM
4:55	13.55	800	117	checked pumping level, clear water
5:00		500		Decreased to 500 GPM

HOWARD PUMP, INC.

PUMP TEST DATA

FIELD REPORT

NAME C. A. Jahake WELL DIAMETER 14" WELL DEPTH 206
 ADDRESS _____ STATIC WATER LEVEL 57
 LOCATION OF WELL Winkley Area PUMP SETTING 140 AIR LINE 140
 DATE OF DRILLING October 1979
 WELL NO. _____ TEST development SHEET 1 OF _____

DATE/TIME	SPECIFIC YIELD (per ft)	DISCHARGE RATE (GPM)	DRAW DOWN (ft)	REMARKS
10/23/79				
9:50 a.m.			57	beginning static water level
10:00		300		begin to surge well 5 times then began
10:10	30.0	300	57	pumping at 300 GPM
				pumped a little fine sand for about 2 minutes
				then cleared
10:15		300		Surged 4 times then continued pumping at 300 GPM
10:25	37.50	300	65	Water became a little milky for 2 minutes
10:30		300		Surged 2 times then remained at a discharge
				rate of 300 GPM
10:40	37.50	300	65	Water remained clear
10:45		300		Surged 3 times then continued at 300 GPM
10:55	37.50	300	65	Water became milky for 2 minutes
11:00		300		Surged well 4 times, then increased to 500 GPM
11:10	33.33	500	72	Water remained clear
11:15		500		Surged well 4 times then resumed at 500 GPM
11:25	33.33	500	72	Water remained milky
11:30		500		Surged well 4 times then continued at 500 GPM
11:40	35.71	500	71	Water milky
11:45		500		Surged 3 times then remained at 500 GPM
11:55	35.71	500	71	Water milky
12:00 noon		500		Surged 4 times then increased discharge rate
				to 800 GPM
12:10	25.80	800	63	Water milky
12:15		800		Surged 3 times then continued at 800 GPM
12:25	24.24	800	90	Water clear
12:30		800		Surged 4 times, remained pumping at 800 GPM
12:40	24.24	800	90	Water clear
12:45		800		Surged 4 times, increased discharge rate to 1000 GPM
				remained at a discharge rate of 1000 GPM
12:55	24.24	1000	90	Water clear
1:00		1000		Surged 4 times, increased well to 1000 GPM
1:10	20.40	1000	106	Water clear
1:15		1000		Surged well 3 times, continued to pump at
				1000 GPM
1:25	20.40	1000	106	Water clear, no sand

HOWARD PUMP, INC.

PUMP TEST DATA

FIELD REPORT

NAME J. L. Jahnke WELL DIAMETER 14" WELL DEPTH 206
 ADDRESS _____ STATIC WATER LEVEL 57
 LOCATION OF WELL _____ PUMP SETTING 180 AIR LINE 160
 WELL NO. _____ DATE OF DRILLING _____
 TEST Development SHEET 2 OF _____

DATE TIME	SPECIFIC YIELD (per ft)	DISCHARGE RATE (GPM)	DRAW DOWN (ft)	REMARKS
10/23/79		1000		Surged 4 times then continued at discharge rate of 1000 GPM
1:40	20.40	1000	106	Water clear, no sand
1:45		1000		Surged 4 times then continue to pump at 1000
1:55	20.40	1000	106	Water clear, no sand
2:00	20.40	1000	106	Continued pumping at a discharge rate of 1000 GPM to begin a 1 hr. check to see if pumping level will drop like yesterday
2:10	19.60	1000	108	
2:20	19.23	1000	109	Adjust throttle to compensate for drawdown
2:30	18.51	1000	111	Water clear, no sand
2:40	18.10	1000	112	Pumping level still dropping
2:50	17.55	1000	114	Pumping level still dropping
3:00		300		Water clear, no sand
3:10	42.05	300	64	Surged 2 times then started step up procedure over again. Beginning at 300 GPM
3:15		300		Water clear after 3 min. milky
3:30		500		Surged well 3 times then began pumped at 300 GPM
3:40	50.00	500	67	Surged well 4 times, increased to 500 GPM
3:45		500		No sand, water milky
3:55	50.00	500	67	Surged 4 times then resumed at 500 GPM
4:00		500		Water milky
4:10	30.76	500	63	Surged well 4 times then increased to 600 GPM
4:15		500		Water milky
4:25	35.33	500	61	Surged 4 times and continued at a discharge rate of 500 GPM
4:30		1000		Water clear, no sand
4:40	28.57	1000	92	Surged 4 times, then increased to 1000 GPM
4:45		1000		Water milky
4:55	27.02	1000	94	Surged well 4 times then continued pumping at 1000 GPM
5:00		1200		Water milky, no sand
				Surged 2 times then increased discharge rate to 1200 GPM to investigate as to whether or not it will pump down at this discharge rate.

HOWARD PUMP, INC.

PUMP TEST DATA
FIELD REPORT

NAME C. R. Jahnke WELL DIAMETER 14" WELL DEPTH 206
 ADDRESS _____ STATIC WATER LEVEL 57
 LOCATION OF WELL _____ PUMP SETTING 180 AIR LINE 168
 DATE OF DRILLING _____
 WELL NO. _____ TEST Development SHEET 1 OF _____

DATE/TIME	SPECIFIC YIELD (per ft)	DISCHARGE RATE (GPM)	DRAW DOWN (ft)	REMARKS
9:25			57	Beginning static water level
9:30		300		Began pumping at a discharge rate of 300 GPM
9:40	42.85	300	64	Water clear, no sand
9:45		300		Surged well 3 times then maintained 300 GPM water became dirty 1 min then cleared up
9:55	60.00	300	62	
10:00		500		Surged 3 times then increased to 500 GPM water pumped milky for 2 min. in no sand
10:10	62.50	500	65	
10:15		500		Surged well 3 times then continued pumping 500 GPM water pumping milky
10:25	62.50	500	65	
10:30		800		Surged well 3 times then increased discharge rate to 800 GPM
10:40	42.10	800	76	Pumping milky
10:45		800		Surged 3 times and continued pumping 800 GPM
10:55	42.10	800	76	Pumped milky
11:00		1000		Surged 3 times, then increased discharge rate to 1000 GPM
11:10	30.46	1000	83	Water pumping milky
11:15		1000		Surged 3 times, then continued to pump 1000GPM
11:25	35.71	1000	85	Water pumped milky
11:30		1200		Surged 3 times then increased to 1200 GPM
11:40	27.27	1200	101	Pumping milky water
11:45		1200		Surged 4 times then continued to pump 1200 GPM
11:55	26.56	1200	102	Water milky
12:00 noon		1200		Start 1 hour pumping test at 1200 GPM
12:10	24.45	1200	106	Water clear
12:20	21.42	1200	113	Adjust throttle to compensate for pumping level dropping
12:30	19.35	1200	119	Pumping clear
12:40	18.46	1200	122	Water clear
12:50	18.46	1200	122	Stabilized
12:55	18.46	1200	122	Remains stabilized
1:00 pm		1300		Increased discharge rate to 1300 GPM
1:10	17.56	1300	131	Checked pumping level and adjusted throttle

STATE OF CALIFORNIA
THE RESOURCES AGENCY
DEPARTMENT OF WATER RESOURCES
WATER WELL DRILLERS REPORT

Do not fill in

No. 223603

ORIGINAL
with DWR

Well of Interest No. 200336
Permit No. or Date 05188304

State Well No. _____
Other Well No. _____

OWNER: Name Curtis R. Jahnke
P.O. Box 6247
Sanga Barbara, CA Zip 93111

LOCATION OF WELL (See instructions):
City San Bernardino Owner's Well Number _____
Address if different from above _____
Map 11N Range 3W Section NE 1/4 of 5
Mile from cities, roads, railroads, fences, etc. _____

(12) WELL LOG: Total depth _____ ft. Depth of completed well _____ ft.

from ft	to ft	Formation (Describe by color, character, size or material)
0	-2	Sand & clay.
2	-3	Boulder.
3	-15	Sand & gravel.
15	-30	Fine sand.
30	-75	Clay.

WELL #3

FIELD #2

(3) TYPE OF WORK:

- New Well Deepening
- Reconstruction
- Reconditioning
- Horizontal Well
- Destruction (Describe destruction materials and procedures in Item 12)

(4) PROPOSED USE:

- Domestic
- Irrigation
- Industrial
- Test Well
- Stocks
- Municipal
- Other

75	-120	Sand & Gravel.
130	-140	Clay & sand.
140	-200	Sand & gravel.
200	-253	Sand & gravel & clay.
253	-263	Sand.
263	-288	Sand & clay.
288	-305	Black lava (hard).
305	-315	Redish-black lava (med-hard).
315	-325	Black lava (hard).

WELL LOCATION SKETCH

- PAINT:
- Reverse
 - Air
 - Bucket

(6) GRAVEL PACK:
Yes No Size _____
Diameter of bore 24"
Packed from 20 to 345 ft.

(8) PERFORATIONS:
Type of perforations or size of screen _____

To ft.	Dia. in.	Gage or Wall	From ft.	To ft.	Slot size
345	14	3/16	95	241	slots
			241	337	louvers
			337	345	slots

325	-330	Redish-blakk lava (med-)hard.
330	-345	Black lava.

WELL SEAL:

Sanitary seal provided? Yes No If yes, to depth 20 ft.
Sealed against pollution? Yes No Interval _____ ft.
If sealing _____ cement

WATER LEVELS:

First water, if known _____ ft.
Level after well completion _____ ft.

WELL TESTS:

Test made? Yes No If yes, by whom? HPI.
Pump Blower Air lift
Water at start of test 47 ft. At end of test 47 ft.
1200 gal/min after 8 hours Water temperature _____
Test made? Yes No If yes, by whom? _____
Log made? Yes No If yes, attach copy to this report

Work started _____ 19 _____ Completed _____ 19 _____

WELL DRILLER'S STATEMENT:

This well was drilled under my supervision and this report is true to the best of my knowledge and belief.

SIGNED Gregg Brown
(Well Driller)
NAME Howard Pump Inc.
(Person, firm, or corporation) (Typed or printed)
Address 28753 W. Hwy 58
City Barstow, CA Zip 92311
License No. 281814 Date of this report May 23, 1983

TEST PUMP DATA
 TEST PUMP DATA
 WELL DESIGNATION INC STATIC WATER LEVEL 47
 WELL DIAMETER 14" AIRLINE 200
 WELL DEPTH 355' PUMP SETTING 200
 Santa Barbara, CA 93111

CURTIS R. JAHNKE
 P.O. Box 6247
 SHEET OF

TIME	SPECIFIC YIELD ()	DISCHARGE RATE ()	DRAW DOWN ()	PUMPING LEVEL ()	REMARKS
00				50	
00:30		500	10	60	Pumping dirty.
00:45		500	10	60	Surge still dirty.
00:00		500	10	60	Surge, still dirty.
00:00		500	8	58	Clearing up.
00:15		500	8	58	Still surging, cleaning up water backing up.
00:00		500	7	57	Clearing up.
00:30		500	7	57	Clearing up, shut down due to water backing up.
00:31-83					
00:30	100	500	5	52	Cloudy for 20 minutes.
00:00	100	500	5	52	
00:15	120	600	5	52	Surged 2 times, cloudy for 5 minutes.
00:30	114.2	800	7	54	Surged 2 times, cloudy for 2 minutes.
00:45	114.2	1000	7	54	
00:00	114.2	1000	7	54	Surged 2 times, cloudy for 2 minutes.
00:15	133.3	1200	9	56	
00:30	133.3	1200	9	56	
00:45	133.3	1200	9	56	Surged 2 times, stayed clean.
00:00	133.3	1200	9	56	
00:15	133.3	1200	9	56	Surged 2 times, stayed clean.
00:30	120	600	5	52	Surged 2 times, stayed clean no sand.
00:45	120	600	5	52	Surged 2 times, stayed clean

ORIGINAL
File with DWR

#4

STATE OF CALIFORNIA
THE RESOURCES AGENCY

DEPARTMENT OF WATER RESOURCES
WATER WELL DRILLERS REPORT

From CJ 7/11/10

11a

Do not fill in

No. 222715

Number of Intent No. 201205
Permit No. or Date 03108301

State Well No. 11N3W5A1
Other Well No.

(1) OWNER: Name Curtis R. Jahnke
Address P.O. Box 6247
City Santa Barbara, CA Zip 93111

(2) LOCATION OF WELL (See instructions):
County San Bernardino Owner's Well Number
Well address if different from above
Township 11N Range 3W Section 5
Distance from cities, roads, railroads, fences, etc.

(12) WELL LOG: Total depth _____ ft. Depth of completed well _____ ft.
from ft. to ft. Formation (Describe by color, character, size or material)
0 - 30 Sand, coarse
30 - 90 Clay
90 - 100 Sand, fine
100 - 130 Sand, Medium
130 - 160 Sand and 5% clay.

NE Quarter
WELL #4

(3) TYPE OF WORK:
New Well Deepening
Reconstruction
Reconditioning
Horizontal Well
Destruction (Describe destruction materials and procedures in Item 12)

(4) PROPOSED USE:
Domestic
Irrigation
Industrial
Test Well
Stock
Municipal
Other

160 - 245 Sand, medium and clay 75%.
245 - 250 Hard, black, lava sand.
250 - 252 Black lava

WELL LOCATION SKETCH

(5) EQUIPMENT:
Rotary Reverse
Cable Air
Other Bucket

(6) GRAVEL PACK:
Yes No Size 24"
Diameter of bore
Packed from 20 to 252

(7) CASING INSTALLED:
Steel Plastic Concrete

(8) PERFORATIONS:
Type of perforation or size of screen

From ft.	To ft.	Dia. in.	Gage or Wall	From ft.	To ft.	Slot size
0	252	14	3/16	95	143	louvers
				143	252	slots

(9) WELL SEAL:
Was surface sanitary seal provided? Yes No If yes, to depth 20 ft.
Were strata sealed against pollution? Yes No Interval _____ ft.
Method of sealing _____

Work started _____ 19 _____ Completed _____ 19 _____

(10) WATER LEVELS:
Depth of first water, if known _____ ft.
Standing level after well completion _____ ft.

WELL DRILLER'S STATEMENT:
This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

(11) WELL TESTS:
Was well test made? Yes No If yes, by whom? _____
Type of test Pump Bailer Air lift
Depth to water at start of test _____ ft. At end of test _____ ft.
Discharge _____ gal/min after _____ hours Water temperature _____
Analysis made? Yes No If yes, by whom? _____
Sonic log made? Yes No If yes, attach copy to this report

SIGNED _____ Gregg Brown (Well Driller)
NAME _____ Howard Pump, Inc. (Person, firm, or corporation) (Typed or printed)
Address _____ 28753 W. Hwy 58
City _____ Barstow, CA Zip 92311
License No. _____ 281814 Date of this report _____ March 16, 1983

HOWLAND PUMP CO.
TEST PUMP DATA

NAME Curtis R. Jahnke WELL DESIGNATION NE¹/₄ STATIC WATER LEVEL 68'
 ADDRESS P.O. Box 6247 WELL DIAMETER 14" AIRLINE 182'
Santa Barbara, CA 93111 WELL DEPTH 252' PUMP SETTING 182'
 LOCATION Hinkley TEST _____ SHEET 2 OF _____

DATE/TIME	SPECIFIC YIELD ()	DISCHARGE RATE ()	DRAW DOWN ()	PUMPING LEVEL ()	REMARKS
3-17-83					
8:30'	2.8	80	28	96	
8:40	2.8	80	28	96	Surged 2 times, cloudy.
8:50	3.3	70	21	89	Surged 2 times, cloudy.
9:00	3.3	70	21	89	Surged 2 times, cloudy.
9:10	3.0	80	26	94	Surged 2 times, cloudy.
9:20	3.0	100	33	101	Surged 2 times, cloudy.
9:30	2.7	100	37	105	Surged 2 times, cloudy.
9:40	2.3	120	51	119	Surged 2 times, stayed clean.
9:50	2.2	120	53	121	Surged 2 times, stayed clean.
10:00	1.6	150	90	158	Surged 2 times, stayed clean.
10:10	1.5	150	100	168	Surged 2 times, stayed clean.
10:20	2.2	80	35	103	Surged 2 times, cloudy.
10:30	2.8	80	28	96	Surged 2 times, cloudy.
10:40	2.8	80	28	96	Surged 2 times, cloudy.
10:50	3.0	80	26	94	Surged 2 times, cloudy.
11:00	2.8	100	35	103	Surged 2 times, stayed clean.
11:15	2.7	100	37	105	Surged 2 times, stayed clean.
11:30	2.7	100	37	105	Surged 2 times, stayed clean.
11:45	2.7	100	37	105	Surged 2 times, stayed clean.
12:00	2.7	100	37	105	Surged 2 times, stayed clean.
12:15	2.6	60	23	91	Surged 2 times, stayed clean.
12:30	2.6	60	23	91	Surged 2 times, cloudy.
12:45	2.6	60	23	91	Surged 2 times, cloudy.
1:00	2.6	60	23	92	Surged 2 times. stayed clean.

ORIGINAL
File with DWR

#6

STATE OF CALIFORNIA
WELL COMPLETION REPORT
Refer to Instruction Pamphlet

DWR USE ONLY - DO NOT FILL IN
11 N 10.3 W 4 S 10.1 S
STATE WELL NO./STATION NO.
LONGITUDE
LATITUDE
APN/TRS/OTHER

Page 1 of 1
Owner's Well No. _____
Date Work Began 7-3-95, Ended 7-5-95
Local Permit Agency San Bernardino County
Permit No. 06199550V Permit Date 6-19-95

No. 550350

WELL OWNER 805 994 3588

DEPTH FROM SURFACE		DESCRIPTION <i>Describe material, grain size, color, etc.</i>
Fl.	to Fl.	
0	2	Top Soil
2	30	Sandy Clay
30	33	Brown Clay
33	35	Sand
35	40	Brown Clay & Gravel
40	45	Clay
45	70	Coarse Sand
70	92	Clay & Sand Stringers
92	100	Coarse Sand
100	170	Clay
170	214	Gravel & Clay Stringers
214	270	D.G. & Volanic Rock
270	313	Clay & Volanic Rock
313	323	Clay
323	402	Volcanic Rock & Clay Stringers
402	410	Clay

Name Oasis Ranch Curt Jahnke
Mailing Address P.O. Box 6247 Santa Barbara, CA 93160
CITY STATE ZIP
WELL LOCATION
Address North of Oasis Rd 2 1/2 Mile, West of Hinkley Rd 1 1/2 Mile
City San Bernadino
County San Bernadino
APN Book 489-161-11 Parcel
Township 11N Range 3 W Section 5
Latitude _____ NORTH Longitude _____ WEST
DEG. MIN. SEC. DEG. MIN. SEC.
LOCATION SKETCH
NORTH
WEST EAST
1 Mile
Oasis
Hinkley Rd.
8 1/2 Mile
Hwy 58
SOUTH
Illustrate or Describe Distance of Well from Landmarks such as Roads, Buildings, Fences, Rivers, etc. PLEASE BE ACCURATE & COMPLETE.
ACTIVITY (X)
X NEW WELL
MODIFICATION/REPAIR
___ Deepen
___ Other (Specify)
DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")
PLANNED USE(S)
(X)
___ MONITORING
WATER SUPPLY
___ Domestic
___ Public
___ Irrigation
___ Industrial
___ "TEST WELL"
___ CATHODIC PROTECTION
___ OTHER (Specify)
DRILLING METHOD Reverse FLUID _____
WATER LEVEL & YIELD OF COMPLETED WELL
DEPTH OF STATIC WATER LEVEL _____ (Fl.) & DATE MEASURED _____
ESTIMATED YIELD _____ (GPM) & TEST TYPE _____
TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Fl.)
* May not be representative of a well's long-term yield.

DEPTH FROM SURFACE Fl. to Fl.	BORE-HOLE DIA. (Inches)	CASING(S)					DEPTH FROM SURFACE Fl. to Fl.	ANNULAR MATERIAL TYPE				
		TYPE (X)	MATERIAL/GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)		CE-MENT (X)	BEN-TONITE (X)	FILL (X)	FILTER PACK (TYPE/SIZE)	
0	140	32"	X	Steel	18"	1/4"	0	40	XX			
140	200	32"	X	Steel	18"	1/4"	0	410		XX	3/8 & 5/16	
200	205	32"	X	Steel	18" to 10" Taper							
205	405	32"	X	Steel	10"	1/2"						
0	40	44"	X	Steel	34"	5/16						

ATTACHMENTS (X)
 ___ Geologic Log
 ___ Well Construction Diagram
 ___ Geophysical Log(s)
 ___ Soil/Water Chemical Analyses
 ___ Other _____
 ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT
 I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.
 NAME Myers Bros. Well Drilling, Inc. RV 4
 (PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)
 ADDRESS 8650 E. Lacey Blvd. Hanford, CA 93230
 CITY STATE ZIP
 Signed Carla Farrell DATE SIGNED 7-12-95 548214
 WELL DRILLER/AUTHORIZED REPRESENTATIVE DATE SIGNED C-57 LICENSE NUMBER



APPENDIX B

WELL PUMP TEST RESULTS Feb/Mar 2011

Source:

Appendix taken directly from a Hydrogeologic Evaluation prepared by Ron Barto Ground Water Consultant in 2011, provided to Schrader Real Estate and Auction Co., Inc. by the Owner.

Oasis Ranch

72-HOUR PUMPING TEST

Drawdown in Adjacent Wells

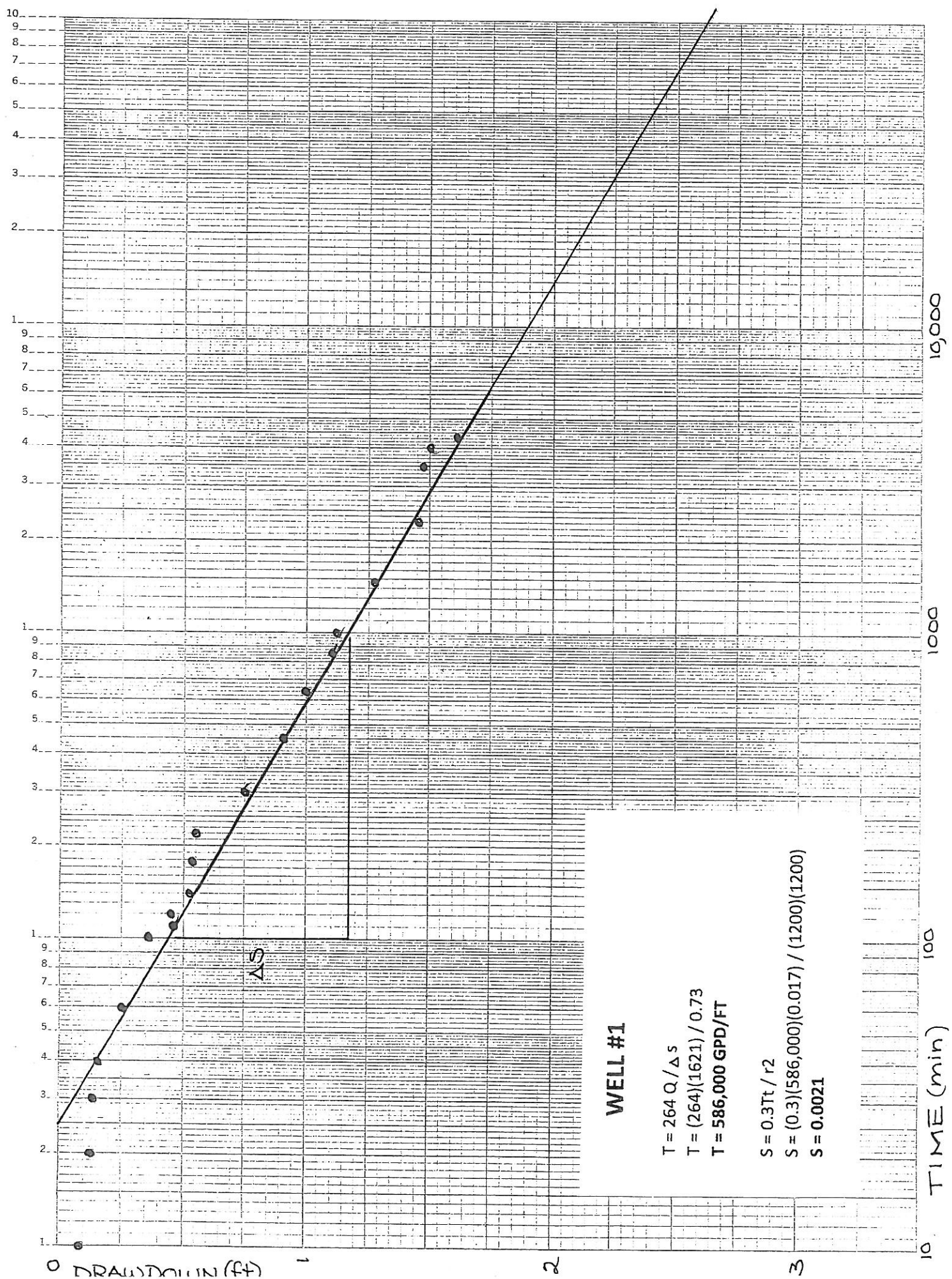
Date	Time	Elapse	Well #1	Well #2	Well #4	Well #5	Well #6
		Time	Drawdown	Drawdown	Drawdown	Drawdown	Drawdown
		(min)	(ft)	(ft)	(ft)	(ft)	(ft)
2/28/2011	13:00	0	0	0	0	0	0
Monday	13:10	10	0.07	0	0	0	0.01
	13:20	20	0.12	0	0	0	0.03
	13:30	30	0.13	0	0	0	0.07
	13:40	40	0.15	0	0	0.02	0.11
	13:50	50	0.17	0	0	0.06	0.17
	14:00	60	0.25	0	0	0.10	0.17
	14:10	70	0.31	0	0	0.10	0.21
	14:20	80	0.29	0	0	0.14	0.23
	14:30	90	0.37	0	0	0.14	0.27
	14:40	100	0.37	0	0	0.20	0.29
	14:50	110	0.45	0	0	0.18	0.31
	15:00	120	0.45	0	0	0.24	0.35
	15:20	140	0.53	0	0	0.26	0.35
	15:40	160	0.55	0	0	0.26	0.41
	16:00	180	0.59	0	0	0.30	0.43
	16:20	200	0.61	0.04	0	0.28	0.47
	16:40	220	0.67	0.05	0	0.36	0.55
	17:10	250	0.69	0.07	0	0.40	0.53
	18:00	300	0.76	0.11	0	0.42	0.62
	18:50	350	0.82	0.15	0	0.42	0.68
	19:40	400	0.86	0.16	0	0.48	0.68
	20:30	450	0.90	0.19	0	0.50	0.68
	21:20	500	0.90	0.21	0	0.52	0.72
	22:10	550	0.96	0.22	0	0.52	0.70
	23:00	600	0.98	0.23	0	0.58	0.64
	23:50	650	1.00	0.24	0	0.58	0.65
3/1/2011	0:40	700	1.02	0.27	0	0.60	0.65
Tuesday	1:30	750	1.10	0.28	0	0.60	0.78
	2:20	800	1.08	0.29	0	0.62	0.76
	3:10	850	1.10	0.29	0	0.60	0.76
	4:00	900	1.12	0.30	0	0.62	0.74
	4:50	950	1.10	0.32	0	0.60	0.84
	5:40	1000	1.12	0.32	0	0.68	0.78
	6:30	1050	1.12	0.32	0	0.67	0.80
	7:20	1100	1.14	0.32	0	0.70	0.80
	8:10	1150	1.12	0.31	0	0.70	0.78
	9:00	1200	1.18	0.31	0	0.70	0.82
	9:50	1250	1.16	0.29	0	0.72	0.82
	10:40	1300	1.18	0.31	0.01	0.71	0.84
	11:30	1350	1.18	0.32	0	0.72	0.84
	12:20	1400	1.22	0.35	0.01	0.74	0.86

Oasis Ranch

72-HOUR PUMPING TEST
 Drawdown in Adjacent Wells

Date	Time	Elapse	Well #1	Well #2	Well #4	Well #5	Well #6
		Time	Drawdown	Drawdown	Drawdown	Drawdown	Drawdown
		(min)	(ft)	(ft)	(ft)	(ft)	(ft)
	13:10	1450	1.28	0.36	0.01	0.74	0.88
	15:10	1570	1.28	0.41	0.02	0.76	0.92
	17:10	1690	1.34	0.44	0.03	0.77	0.94
	19:10	1810	1.34	0.46	0.02	0.80	0.90
	21:10	1930	1.38	0.47	0.04	0.82	0.94
	23:10	2050	1.36	0.47	0.05	0.83	0.94
3/2/2011	1:10	2170	1.40	0.47	0.05	0.82	0.94
Wednesday	3:10	2290	1.42	0.49	0.04	0.83	0.96
	5:10	2410	1.44	0.48	0.06	0.83	0.98
	7:10	2530	1.42	0.47	0.05	0.85	0.94
	9:10	2650	1.42	0.49	0.05	0.84	1.00
	11:10	2770	1.42	0.45	0.06	0.87	0.98
	13:10	2890	1.44	0.46	0.07	0.88	0.98
	15:10	3010	1.46	0.50	0.07	0.91	1.02
	17:10	3130	1.49	0.52	0.08	0.90	1.04
	19:10	3250	1.48	0.53	0.08	0.90	1.08
	21:10	3370	1.48	0.53	0.08	0.90	1.02
	23:10	3490	1.48	0.50	0.09	0.92	1.04
3/3/2011	1:10	3610	1.49	0.50	0.09	0.92	1.02
Thursday	3:10	3730	1.48	0.50	0.10	0.90	1.04
	5:10	3850	1.51	0.51	0.10	0.92	1.04
	7:10	3970	1.51	0.51	0.09	0.94	1.04
	9:10	4090	1.53	0.51	0.11	0.94	1.08
	11:10	4210	1.58	0.51	0.11	0.92	1.08
	13:00	4320	1.61	0.52	0.12	0.96	1.10

4920	0.55	0.26	0.13	0.33	0.39
4970	0.53	0.25	0.13	0.32	0.37
5020	0.51	0.26	0.14	0.33	0.31
5070	0.45	0.24	0.14	0.31	0.31
5120	0.43	0.21	0.14	0.34	0.27
5170	0.39	0.20	0.14	0.33	0.27
5220	0.37	0.20	0.14	0.31	0.25
5270	0.37	0.18	0.14	0.28	0.25
5320	0.31	0.16	0.13	0.28	0.21
5370	0.33	0.17	0.13	0.25	0.17
5420	0.31	0.15	0.13	0.23	0.17
5470	0.27	0.15	0.13	0.21	0.13
5520	0.26	0.13	0.13	0.2	0.17
5570	0.27	0.13	0.12	0.16	0.17
5620	0.27	0.15	0.12	0.16	0.13
5670	0.27	0.14	0.12	0.15	0.13



WELL #1

- T = 264 Q / Δs
- T = (264)(1621) / 0.73
- T = 586,000 GPD/FT
- S = 0.3Tt / r²
- S = (0.3)(586,000)(0.017) / (1200)(1200)
- S = 0.0021

OASIS WELL #1

DATE	TIME	ELAPSE	TRANSDUCER	DRAWDOWN	RECOVERY	COMMENTS
	(hr:min)	(min)	READING (feet)	S (feet)	S' (feet)	
2/28/2011	12:50		69.00			SWL = 69 feet
	13:00	0	69.00	0		WELL #3 ON
Monday	13:10	10	69.07	0.07		
	13:20	20	69.12	0.12		
	13:30	30	69.13	0.13		
	13:40	40	69.15	0.15		
	13:50	50	69.17	0.17		
	14:00	60	69.25	0.25		
	14:10	70	69.31	0.31		
	14:20	80	69.29	0.29		
	14:30	90	69.37	0.37		
	14:40	100	69.37	0.37		
	14:50	110	69.45	0.45		
	15:00	120	69.45	0.45		
	15:20	140	69.53	0.53		
	15:40	160	69.55	0.55		
	16:00	180	69.59	0.59		
	16:20	200	69.61	0.61		
	16:40	220	69.67	0.67		
	17:10	250	69.69	0.69		
	18:00	300	69.76	0.76		
	18:50	350	69.82	0.82		
	19:40	400	69.86	0.86		
	20:30	450	69.90	0.90		
	21:20	500	69.90	0.90		
	22:10	550	69.96	0.96		
	23:00	600	69.98	0.98		
	23:50	650	70.00	1.00		
3/1/2011	0:40	700	70.02	1.02		
Tuesday	1:30	750	70.10	1.10		
	2:20	800	70.08	1.08		
	3:10	850	70.10	1.10		
	4:00	900	70.12	1.12		
	4:50	950	70.10	1.10		
	5:40	1000	70.12	1.12		
	6:30	1050	70.12	1.12		
	7:20	1100	70.14	1.14		
	8:10	1150	70.12	1.12		
	9:00	1200	70.18	1.18		
	9:50	1250	70.16	1.16		
	10:40	1300	70.18	1.18		

OASIS WELL #1

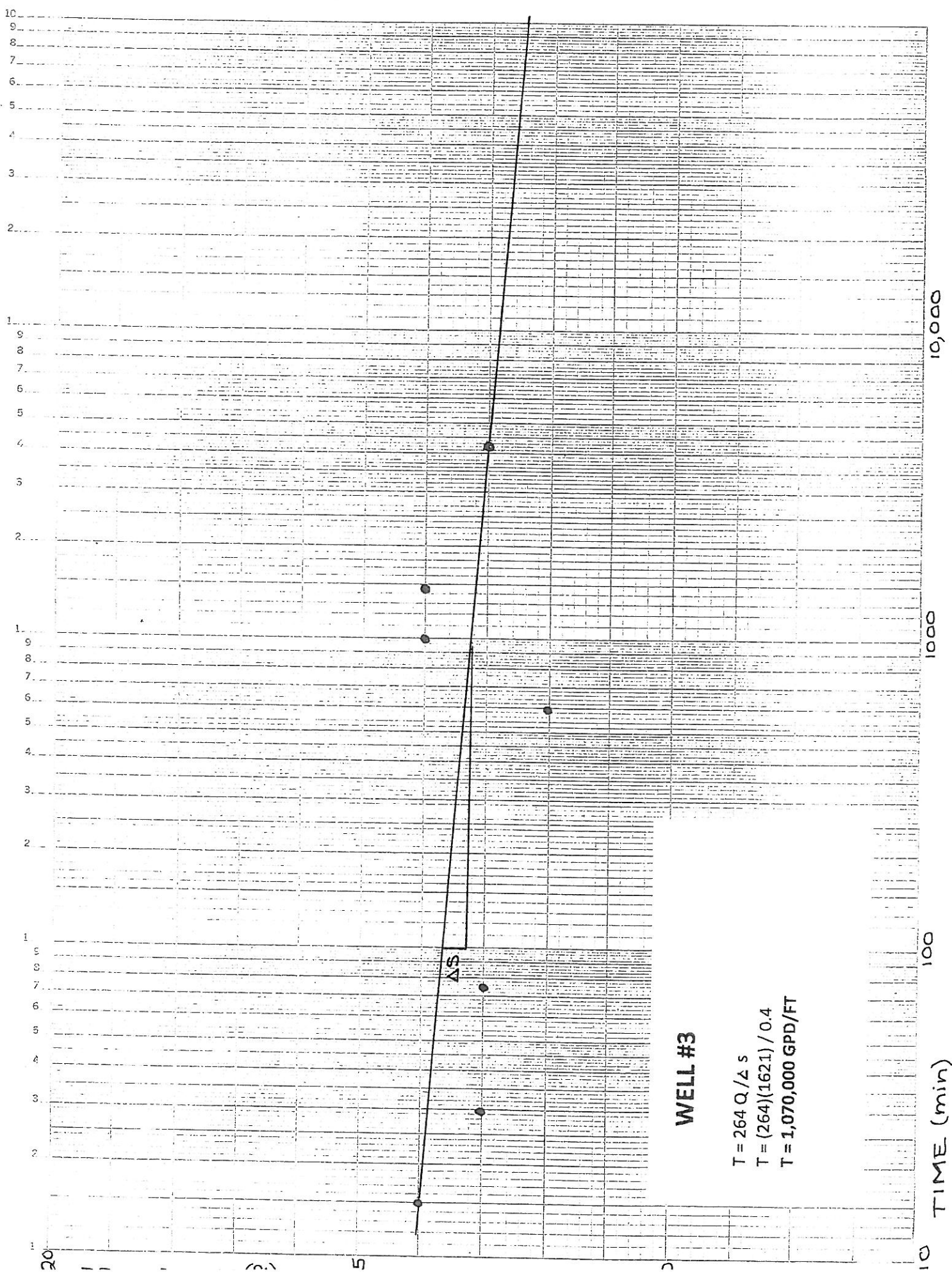
DATE	TIME	ELAPSE	TRANSDUCER	DRAWDOWN	RECOVERY		COMMENTS
		TIME	READING	S	S'		
	(hr:min)	(min)	(feet)	(feet)	(feet)		
	11:30	1350	70.18	1.18			73% of total DD
	12:20	1400	70.22	1.22			
	13:10	1450	70.28	1.28			
	15:10	1570	70.28	1.28			
	17:10	1690	70.34	1.34			
	19:10	1810	70.34	1.34			
	21:10	1930	70.38	1.38			
	23:10	2050	70.36	1.36			
3/2/2011	1:10	2170	70.40	1.40			
Wednesday	3:10	2290	70.42	1.42			
	5:10	2410	70.44	1.44			
	7:10	2530	70.42	1.42			
	9:10	2650	70.42	1.42			
	11:10	2770	70.42	1.42			
	13:10	2890	70.44	1.44			
	15:10	3010	70.46	1.46			
	17:10	3130	70.49	1.49			
	19:10	3250	70.48	1.48			
	21:10	3370	70.48	1.48			
	23:10	3490	70.48	1.48			
3/3/2011	1:10	3610	70.49	1.49			
Thursday	3:10	3730	70.48	1.48			
	5:10	3850	70.51	1.51			
	7:10	3970	70.51	1.51			
	9:10	4090	70.53	1.53			
	11:10	4210	70.58	1.58			
	13:00	4320	70.61	1.61			Well #3 off
							RECOVERY
	13:00		70.61	1.61	0		
	13:10	4330	70.49	1.49	0.12		
	13:20	4340	70.49	1.49	0.12		
	13:30	4350	70.42	1.42	0.19		
	13:40	4360	70.40	1.40	0.21		
	13:50	4370	70.38	1.38	0.23		
	14:00	4380	70.30	1.30	0.31		
	14:10	4390	70.28	1.28	0.33		
	14:20	4400	70.22	1.22	0.39		
	14:30	4410	70.22	1.22	0.39		
	14:40	4420	70.14	1.14	0.47		
	14:50	4430	70.12	1.12	0.49		
	15:00	4440	70.10	1.10	0.51		

OASIS WELL #2

DATE	TIME	ELAPSE	TRANSDUCER	DRAWDOWN	RECOVERY		COMMENTS
		TIME	READING	S	S'		
	(hr:min)	(min)	(feet)	(feet)	(feet)		
2/28/2011	12:20		82.27				SWL = 82.27 feet
	13:00	0	82.27	0			WELL #3 ON
Monday	13:10	10	82.27	0			
	13:20	20	82.27	0			
	13:30	30	82.27	0			
	13:40	40	82.27	0			
	13:50	50	82.27	0			
	14:00	60	82.27	0			
	14:10	70	82.27	0			
	14:20	80	82.27	0			
	14:30	90	82.27	0			
	14:40	100	82.27	0			
	14:50	110	82.27	0			
	15:00	120	82.27	0			
	15:20	140	82.27	0			
	15:40	160	82.27	0			
	16:00	180	82.27	0			
	16:20	200	82.31	0.04			
	16:40	220	82.32	0.05			
	17:10	250	82.34	0.07			
	18:00	300	82.38	0.11			
	18:50	350	82.42	0.15			
	19:40	400	82.43	0.16			
	20:30	450	82.46	0.19			
	21:20	500	82.48	0.21			
	22:10	550	82.49	0.22			
	23:00	600	82.5	0.23			
	23:50	650	82.51	0.24			
3/1/2011	0:40	700	82.54	0.27			
Tuesday	1:30	750	82.55	0.28			
	2:20	800	82.56	0.29			
	3:10	850	82.56	0.29			
	4:00	900	82.57	0.30			
	4:50	950	82.59	0.32			
	5:40	1000	82.59	0.32			
	6:30	1050	82.59	0.32			
	7:20	1100	82.59	0.32			
	8:10	1150	82.58	0.31			
	9:00	1200	82.58	0.31			
	9:50	1250	82.56	0.29			
	10:40	1300	82.58	0.31			

OASIS WELL #2

DATE	TIME	ELAPSE	TRANSDUCER	DRAWDOWN	RECOVERY		COMMENTS
		TIME	READING	S	S'		
	(hr:min)	(min)	(feet)	(feet)	(feet)		
	11:30	1350	82.59	0.32			62% of total DD
	12:20	1400	82.62	0.35			
	13:10	1450	82.63	0.36			
	15:10	1570	82.68	0.41			
	17:10	1690	82.71	0.44			
	19:10	1810	82.73	0.46			
	21:10	1930	82.74	0.47			
	23:10	2050	82.74	0.47			
3/2/2011	1:10	2170	82.74	0.47			
Wednesday	3:10	2290	82.76	0.49			
	5:10	2410	82.75	0.48			
	7:10	2530	82.74	0.47			
	9:10	2650	82.76	0.49			
	11:10	2770	82.72	0.45			
	13:10	2890	82.73	0.46			
	15:10	3010	82.77	0.50			
	17:10	3130	82.79	0.52			
	19:10	3250	82.80	0.53			
	21:10	3370	82.80	0.53			
	23:10	3490	82.77	0.50			
3/3/2011	1:10	3610	82.77	0.50			
Thursday	3:10	3730	82.77	0.50			
	5:10	3850	82.78	0.51			
	7:10	3970	82.78	0.51			
	9:10	4090	82.78	0.51			
	11:10	4210	82.78	0.51			
	13:00	4320	82.79	0.52			Well #3 off
							RECOVERY
	13:00		82.79	0.52	0.00		
	13:10	4330	82.79	0.52	0.00		
	13:20	4340	82.79	0.52	0.00		
	13:30	4350	82.79	0.52	0.00		
	13:40	4360	82.79	0.52	0.00		
	13:50	4370	82.79	0.52	0.00		
	14:00	4380	82.79	0.52	0.00		
	14:10	4390	82.79	0.52	0.00		
	14:20	4400	82.80	0.53	-0.01		
	14:30	4410	82.80	0.53	-0.01		
	14:40	4420	82.79	0.52	0.00		
	14:50	4430	82.81	0.54	-0.02		
	15:00	4440	82.81	0.54	-0.02		



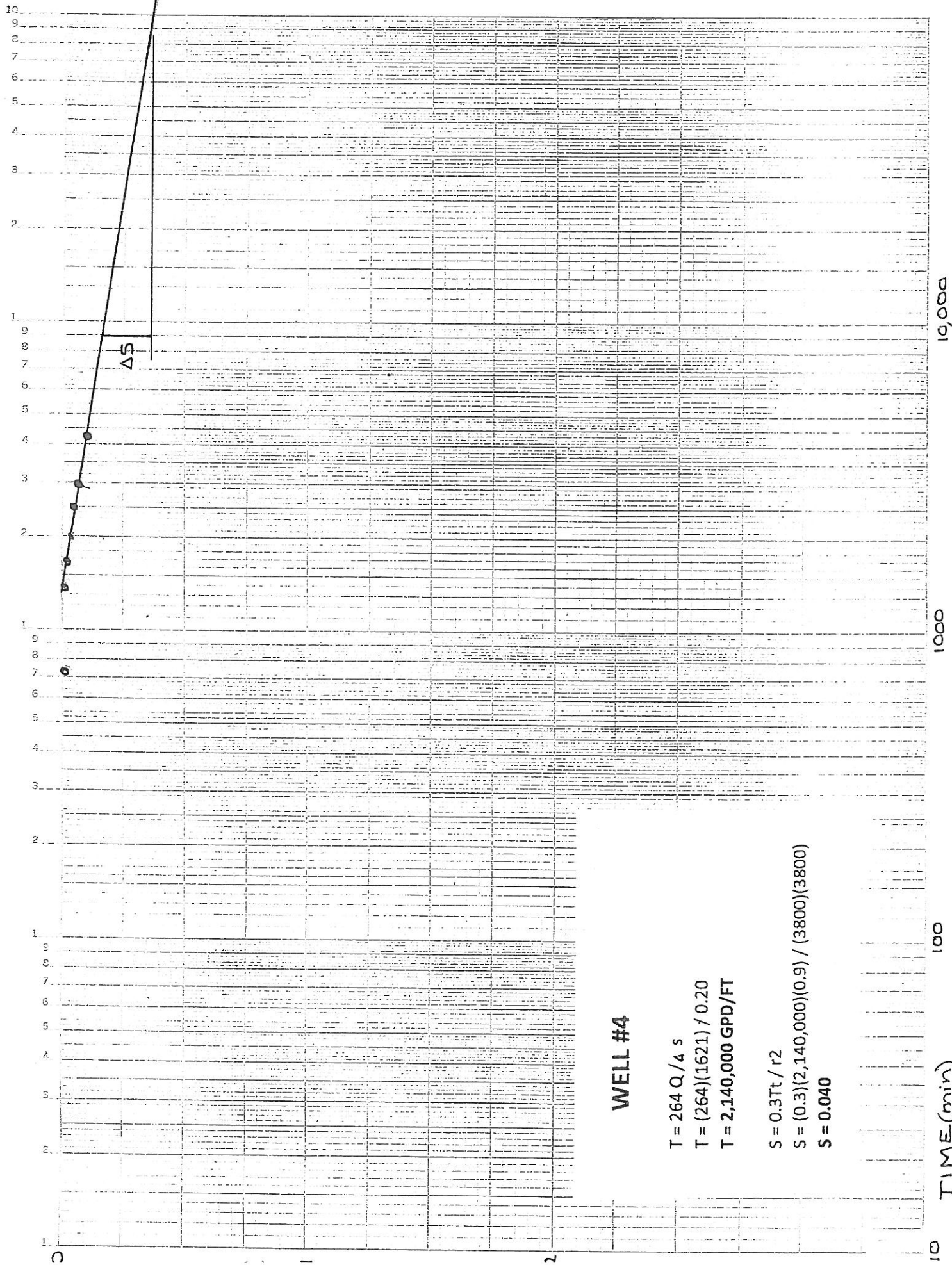
WELL #3

- T = 264 Q / Δ S
- T = (264)(1621) / 0.4
- T = 1,070,000 GPD/FT

DATE	TIME	ELAPSE	ELECT. PROBE	DRAWDOWN	FLOW	FLOW	Q/S	COMMENTS
		TIME	READING	S	READING	Q		
	(hr:min)	(min)	(feet)	(feet)	(gal x 100)	(gpm x 100)	(gpm/ft)	
2/28/2011	12:30		74			0		SWL = 74 feet
	13:00	0	74		28,014			Pump on
	13:15	15	100	26	28,250	15.73		
	13:30	30	101	27	28,488	15.87		
	13:45	45	101	27	28,753	17.67		
	14:15	75	101	27	29,223	15.67		
	14:45	105			29,711	16.27		
	16:15	195			31,195	16.49		
	17:00	240			31,905	15.78		
	18:30	330			33,367	16.24		
	19:00	360			33,777	13.67		
	19:15	375			34,107	22.00		
	20:00	420			34,827	16.00		
	20:30	450			35,320	16.43		
	21:00	480			35,850	17.67		
	21:35	515			36,374	14.97		
	22:00	540			36,779	16.20		
	22:34	574			37,370	17.38		
	23:01	601	102	28	37,800	15.93		
	23:35	635			38,370	16.76		
	23:40	640			38,449	15.80		
	23:59	659			38,762	16.47		
3/1/2011	0:14	674			39,019	17.13		
	0:28	688			39,248	16.36		
	0:44	704			39,518	16.88		
	1:00	720			39,760	15.13		
	1:25	745			40,190	17.20		
	1:53	773			40,635	15.89		
	2:43	823			41,470	16.70		
	3:30	870			42,230	16.17		
	3:50	890			42,552	16.10		
	4:20	920			43,028	15.87		
	4:50	950			43,538	17.00		
	5:20	980			44,000	15.40		
	6:50	1070	100	26	45,567	17.41		
	7:12	1092	100	26	45,790	10.14		
	7:21	1101	100	26	45,932	15.78		
	7:51	1131	100	26	46,411	15.97		
	8:21	1161	100	26	46,890	15.97		
	8:51	1191	100	26	47,372	16.07		
	9:21	1221	100	26	47,856	16.13		
	9:51	1251	100	26	48,339	16.10		
	10:21	1281	100	26	48821	16.07		
	10:51	1311	100	26	49307	16.20		
	11:21	1341	100	26	49802	16.50		
	11:51	1371	100	26	50301	16.63		
	12:21	1401	100	26	50801	16.67		
	12:51	1431	100	26	51299	16.60		
	13:21	1461	100	26	51778	15.97		
	14:21	1521			52738	16.00		
	15:00	1560			53373	16.28		
	16:00	1620			54310	15.62		
	17:00	1680			55247	15.62		
	18:00	1740			56270	17.05		
	18:58	1798			57160	15.34		

RON BARTO GROUND WATER CONSULTANT

16 6010



WELL #4

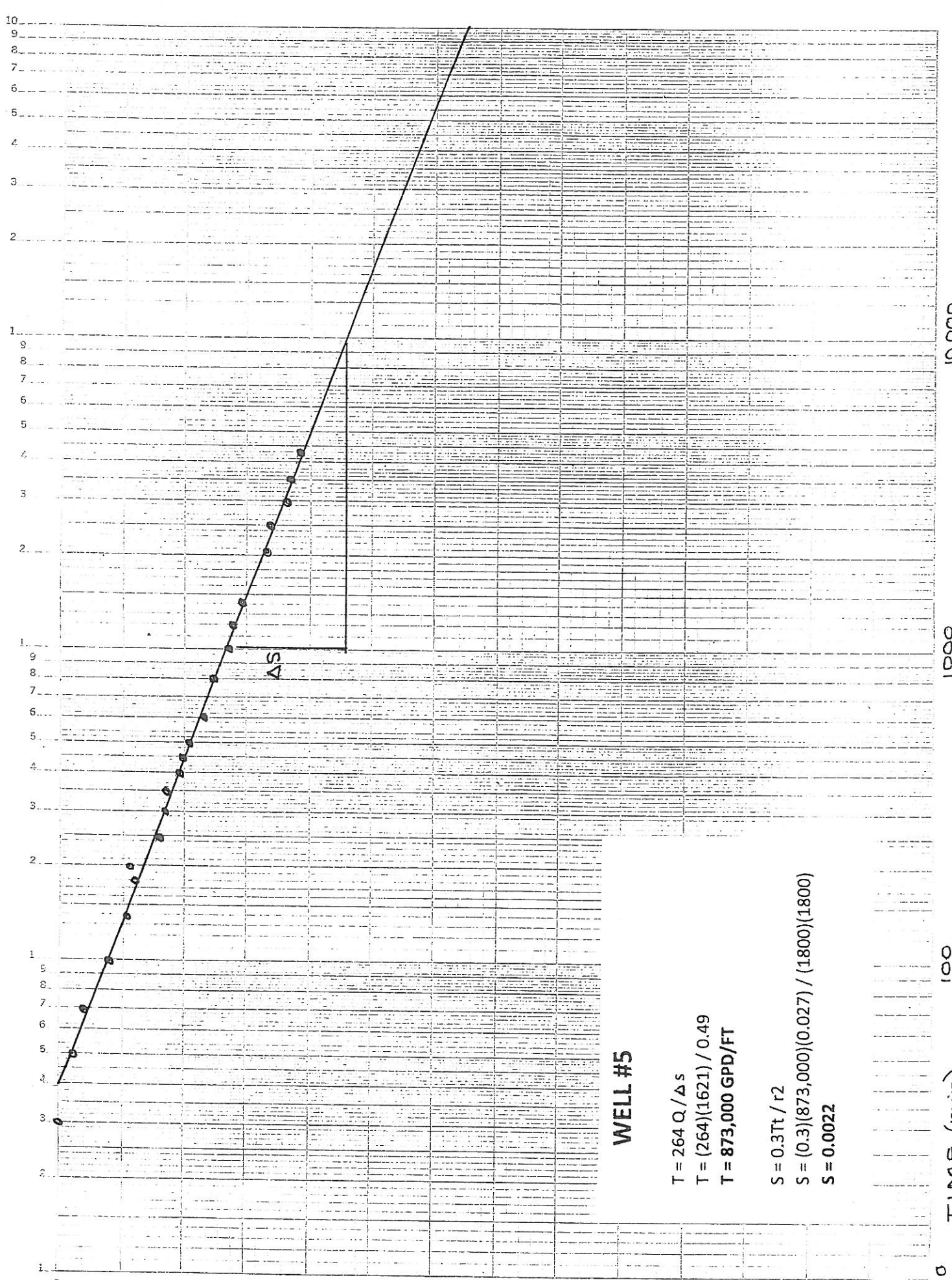
- T = 264 Q / 4 S
- T = (264)(1621) / 0.20
- T = 2,140,000 GPD/FT
- S = 0.3Tt / r2
- S = (0.3)(2,140,000)(0.9) / (3800)(3800)
- S = 0.040

OASIS WELL #4

DATE	TIME	ELAPSE	TRANSDUCER	DRAWDOWN	RECOVERY	COMMENTS
		TIME	READING	S	S'	
	(hr:min)	(min)	(feet)	(feet)	(feet)	
2/28/2011	12:00		91.15			SWL = 91.15 feet
	13:00	0	91.15	0		WELL #3 ON
Monday	13:10	10	91.15	0		
	13:20	20	91.15	0		
	13:30	30	91.15	0		
	13:40	40	91.15	0		
	13:50	50	91.15	0		
	14:00	60	91.15	0		
	14:10	70	91.15	0		
	14:20	80	91.15	0		
	14:30	90	91.15	0		
	14:40	100	91.15	0		
	14:50	110	91.15	0		
	15:00	120	91.15	0		
	15:20	140	91.15	0		
	15:40	160	91.15	0		
	16:00	180	91.15	0		
	16:20	200	91.15	0		
	16:40	220	91.15	0		
	17:10	250	91.15	0		
	18:00	300	91.15	0		
	18:50	350	91.15	0		
	19:40	400	91.15	0		
	20:30	450	91.15	0		
	21:20	500	91.15	0		
	22:10	550	91.15	0		
	23:00	600	91.15	0		
	23:50	650	91.15	0		
3/1/2011	0:40	700	91.15	0		
Tuesday	1:30	750	91.15	0		
	2:20	800	91.15	0		
	3:10	850	91.15	0		
	4:00	900	91.15	0		
	4:50	950	91.15	0		
	5:40	1000	91.15	0		
	6:30	1050	91.15	0		
	7:20	1100	91.15	0		
	8:10	1150	91.15	0		
	9:00	1200	91.15	0		
	9:50	1250	91.15	0		
	10:40	1300	91.16	0.01		

OASIS WELL #4

DATE	TIME	ELAPSE	TRANSDUCER	DRAWDOWN	RECOVERY		COMMENTS
		TIME	READING	S	S'		
	(hr:min)	(min)	(feet)	(feet)	(feet)		
	11:30	1350	91.15	0			
	12:20	1400	91.16	0.01			
	13:10	1450	91.16	0.01			
	15:10	1570	91.17	0.02			
	17:10	1690	91.18	0.03			
	19:10	1810	91.17	0.02			
	21:10	1930	91.19	0.04			
	23:10	2050	91.20	0.05			
3/2/2011	1:10	2170	91.20	0.05			
Wednesday	3:10	2290	91.19	0.04			
	5:10	2410	91.21	0.06			
	7:10	2530	91.20	0.05			
	9:10	2650	91.20	0.05			
	11:10	2770	91.21	0.06			
	13:10	2890	91.22	0.07			
	15:10	3010	91.22	0.07			
	17:10	3130	91.23	0.08			
	19:10	3250	91.23	0.08			
	21:10	3370	91.23	0.08			
	23:10	3490	91.24	0.09			
3/3/2011	1:10	3610	91.24	0.09			
Thursday	3:10	3730	91.25	0.10			
	5:10	3850	91.25	0.10			
	7:10	3970	91.24	0.09			
	9:10	4090	91.26	0.11			
	11:10	4210	91.26	0.11			
	13:00	4320	91.27	0.12			Well #3 off
							RECOVERY
	13:00		91.27	0.12	0.00		
	13:10	4330	91.27	0.12	0.00		
	13:20	4340	91.27	0.12	0.00		
	13:30	4350	91.27	0.12	0.00		
	13:40	4360	91.27	0.12	0.00		
	13:50	4370	91.27	0.12	0.00		
	14:00	4380	91.27	0.12	0.00		
	14:10	4390	91.27	0.12	0.00		
	14:20	4400	91.27	0.12	0.00		
	14:30	4410	91.27	0.12	0.00		
	14:40	4420	91.27	0.12	0.00		
	14:50	4430	91.28	0.13	-0.01		
	15:00	4440	91.28	0.13	-0.01		



WELL #5

- T = 264 Q / Δs
- T = (264)(1621) / 0.49
- T = 873,000 GPD/FT
- S = 0.3Tt / r²
- S = (0.3)(873,000)(0.027) / (1800)(1800)
- S = 0.0022

10 TIME (min)

100

1000

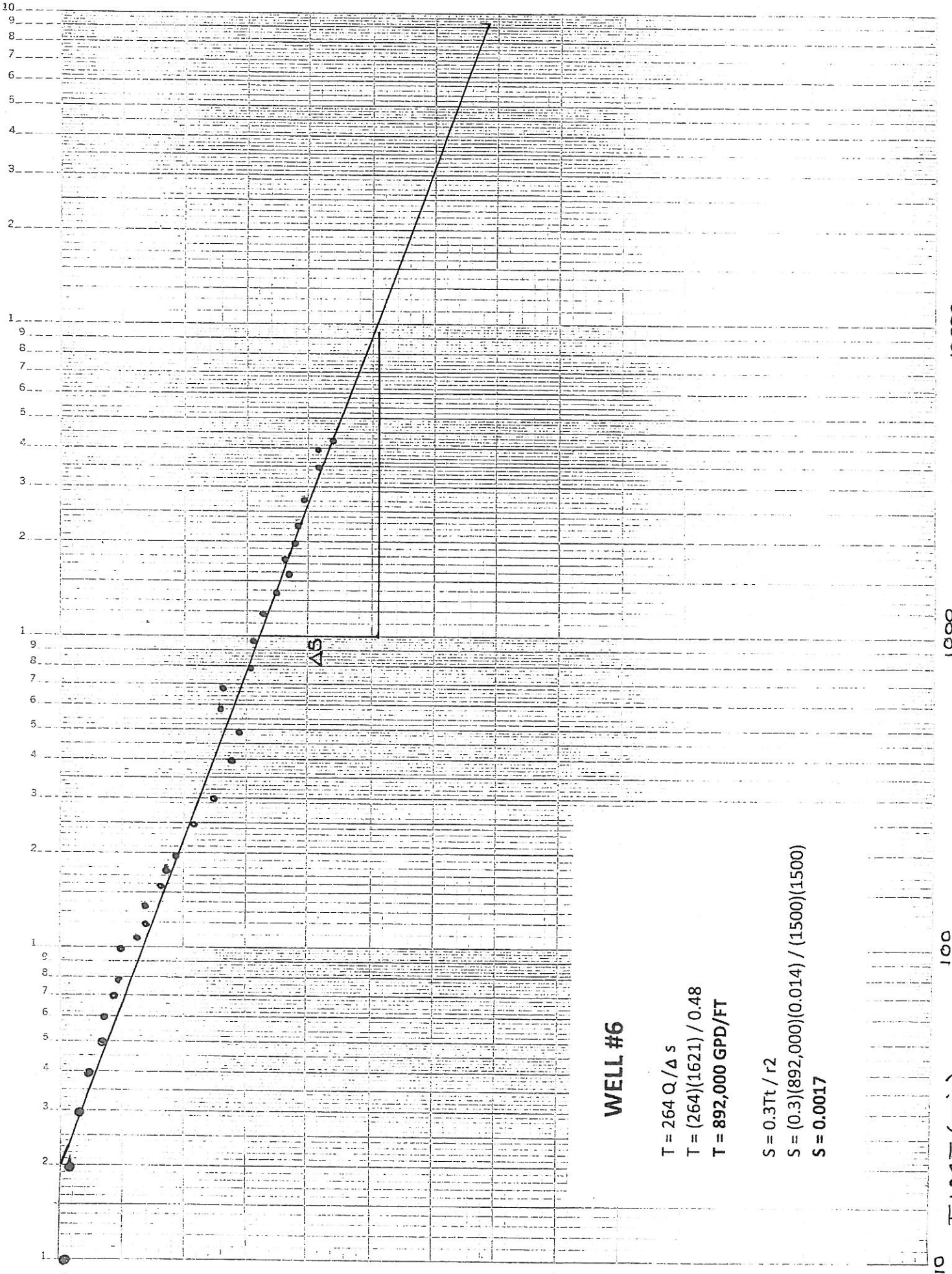
10,000

OASIS WELL #5

DATE	TIME	ELAPSE	TRANSDUCER	DRAWDOWN	RECOVERY		COMMENTS
		TIME	READING	S	S'		
	(hr:min)	(min)	(feet)	(feet)	(feet)		
2/28/2011	12:10		79.95				SWL = 79.95 feet
	13:00	0	79.95	0			WELL #3 ON
Monday	13:10	10	79.95	0			
	13:20	20	79.95	0			
	13:30	30	79.95	0			
	13:40	40	79.97	0.02			
	13:50	50	80.01	0.06			
	14:00	60	80.05	0.10			
	14:10	70	80.05	0.10			
	14:20	80	80.09	0.14			
	14:30	90	80.09	0.14			
	14:40	100	80.15	0.20			
	14:50	110	80.13	0.18			
	15:00	120	80.19	0.24			
	15:20	140	80.21	0.26			
	15:40	160	80.21	0.26			
	16:00	180	80.25	0.30			
	16:20	200	80.23	0.28			
	16:40	220	80.31	0.36			
	17:10	250	80.35	0.40			
	18:00	300	80.37	0.42			
	18:50	350	80.37	0.42			
	19:40	400	80.43	0.48			
	20:30	450	80.45	0.50			
	21:20	500	80.47	0.52			
	22:10	550	80.47	0.52			
	23:00	600	80.53	0.58			
	23:50	650	80.53	0.58			
3/1/2011	0:40	700	80.55	0.60			
Tuesday	1:30	750	80.55	0.60			
	2:20	800	80.57	0.62			
	3:10	850	80.55	0.60			
	4:00	900	80.57	0.62			
	4:50	950	80.55	0.60			
	5:40	1000	80.63	0.68			
	6:30	1050	80.62	0.67			
	7:20	1100	80.65	0.70			
	8:10	1150	80.65	0.70			
	9:00	1200	80.65	0.70			
	9:50	1250	80.67	0.72			
	10:40	1300	80.66	0.71			

OASIS WELL #5

DATE	TIME	ELAPSE	TRANSDUCER	DRAWDOWN	RECOVERY	COMMENTS
		TIME	READING	S	S'	
	(hr:min)	(min)	(feet)	(feet)	(feet)	
	11:30	1350	80.69	0.74		
	12:20	1400	80.71	0.76		
	13:10	1450	80.69	0.74		
	15:10	1570	80.71	0.76		
	17:10	1690	80.72	0.77		
	19:10	1810	80.75	0.80		
	21:10	1930	80.77	0.82		
	23:10	2050	80.78	0.83		
3/2/2011	1:10	2170	80.77	0.82		
Wednesday	3:10	2290	80.78	0.83		
	5:10	2410	80.78	0.83		
	7:10	2530	80.80	0.85		
	9:10	2650	80.79	0.84		
	11:10	2770	80.82	0.87		
	13:10	2890	80.83	0.88		
	15:10	3010	80.86	0.91		
	17:10	3130	80.85	0.90		
	19:10	3250	80.85	0.90		
	21:10	3370	80.85	0.90		
	23:10	3490	80.87	0.92		
3/3/2011	1:10	3610	80.87	0.92		
Thursday	3:10	3730	80.85	0.90		
	5:10	3850	80.87	0.92		
	7:10	3970	80.89	0.94		
	9:10	4090	80.89	0.94		
	11:10	4210	80.87	0.92		
	13:00	4320	80.91	0.96		Well #3 off
						RECOVERY
	13:00		80.90	0.95	0.01	
	13:10	4330	80.93	0.98	-0.02	
	13:20	4340	80.93	0.98	-0.02	
	13:30	4350	80.91	0.96	0	
	13:40	4360	80.90	0.95	0.01	
	13:50	4370	80.86	0.91	0.05	
	14:00	4380	80.83	0.88	0.08	
	14:10	4390	80.79	0.84	0.12	
	14:20	4400	80.77	0.82	0.14	
	14:30	4410	80.74	0.79	0.17	
	14:40	4420	80.70	0.75	0.21	
	14:50	4430	80.67	0.72	0.24	
	15:00	4440	80.66	0.71	0.25	



WELL #6

- T = 264 Q / Δs
- T = (264)(1621) / 0.48
- T = 892,000 GPD/FT
- S = 0.3Tt / r²
- S = (0.3)(892,000)(0.014) / (1500)(1500)
- S = 0.0017

TIME (min)

OASIS WELL #6

DATE	TIME	ELAPSE	TRANSDUCER	DRAWDOWN	RECOVERY	COMMENTS
		TIME	READING	S	S'	
	(hr:min)	(min)	(feet)	(feet)	(feet)	
2/28/2011	12:40		76.55			SWL = 76.55 feet
	13:00	0	76.55	0		WELL #3 ON
Monday	13:10	10	76.56	0.01		
	13:20	20	76.58	0.03		
	13:30	30	76.62	0.07		
	13:40	40	76.66	0.11		
	13:50	50	76.72	0.17		
	14:00	60	76.72	0.17		
	14:10	70	76.76	0.21		
	14:20	80	76.78	0.23		
	14:30	90	76.82	0.27		
	14:40	100	76.84	0.29		
	14:50	110	76.86	0.31		
	15:00	120	76.90	0.35		
	15:20	140	76.90	0.35		
	15:40	160	76.96	0.41		
	16:00	180	76.98	0.43		
	16:20	200	77.02	0.47		
	16:40	220	77.10	0.55		
	17:10	250	77.08	0.53		
	18:00	300	77.17	0.62		
	18:50	350	77.23	0.68		
	19:40	400	77.23	0.68		
	20:30	450	77.23	0.68		
	21:20	500	77.27	0.72		
	22:10	550	77.25	0.70		
	23:00	600	77.19	0.64		
	23:50	650	77.20	0.65		
3/1/2011	0:40	700	77.20	0.65		
Tuesday	1:30	750	77.33	0.78		
	2:20	800	77.31	0.76		
	3:10	850	77.31	0.76		
	4:00	900	77.29	0.74		
	4:50	950	77.39	0.84		
	5:40	1000	77.33	0.78		
	6:30	1050	77.35	0.80		
	7:20	1100	77.35	0.80		
	8:10	1150	77.33	0.78		
	9:00	1200	77.37	0.82		
	9:50	1250	77.37	0.82		
	10:40	1300	77.39	0.84		

OASIS WELL #6

DATE	TIME	ELAPSE	TRANSDUCER	DRAWDOWN	RECOVERY		COMMENTS
		TIME	READING	S	S'		
	(hr:min)	(min)	(feet)	(feet)	(feet)		
	11:30	1350	77.39	0.84			76% of total dd
	12:20	1400	77.41	0.86			
	13:10	1450	77.43	0.88			
	15:10	1570	77.47	0.92			
	17:10	1690	77.49	0.94			
	19:10	1810	77.45	0.90			
	21:10	1930	77.49	0.94			
	23:10	2050	77.49	0.94			
3/2/2011	1:10	2170	77.49	0.94			
Wednesday	3:10	2290	77.51	0.96			
	5:10	2410	77.53	0.98			
	7:10	2530	77.49	0.94			
	9:10	2650	77.55	1.00			
	11:10	2770	77.53	0.98			
	13:10	2890	77.53	0.98			
	15:10	3010	77.57	1.02			
	17:10	3130	77.59	1.04			
	19:10	3250	77.63	1.08			
	21:10	3370	77.57	1.02			
	23:10	3490	77.59	1.04			
3/3/2011	1:10	3610	77.57	1.02			
Thursday	3:10	3730	77.59	1.04			
	5:10	3850	77.59	1.04			
	7:10	3970	77.59	1.04			
	9:10	4090	77.63	1.08			
	11:10	4210	77.63	1.08			
	13:00	4320	77.65	1.10			Well #3 off
							RECOVERY
	13:00		77.65	1.10	0.00		
	13:10	4330	77.65	1.10	0.00		
	13:20	4340	77.59	1.04	0.06		
	13:30	4350	77.53	0.98	0.12		
	13:40	4360	77.51	0.96	0.14		
	13:50	4370	77.49	0.94	0.16		
	14:00	4380	77.49	0.94	0.16		
	14:10	4390	77.47	0.92	0.18		
	14:20	4400	77.41	0.86	0.24		
	14:30	4410	77.39	0.84	0.26		
	14:40	4420	77.37	0.82	0.28		
	14:50	4430	77.37	0.82	0.28		
	15:00	4440	77.33	0.78	0.32		

APPENDIX C

LABORATORY WATER QUALITY REPORTS

Source:

Appendix taken directly from a Hydrogeologic Evaluation prepared by Ron Barto Ground Water Consultant in 2011, provided to Schrader Real Estate and Auction Co., Inc. by the Owner.

APPENDIX D

WELL #6 E-LOG JUNE 1996

Source:

Appendix taken directly from a Hydrogeologic Evaluation prepared by Ron Barto Ground Water Consultant in 2011, provided to Schrader Real Estate and Auction Co., Inc. by the Owner.

GEO-HYDRO-DATA

INCORPORATED

GROUNDWATER LOG

COMPANY : OASIS RANCH
WELL : 6- 95
LOCATION/FIELD : HINKLEY
COUNTY : SAN BERNARDINO
STATE : CALIFORNIA
SECTION :

OTHER SERVICES:
INVOICE
9624
1,000 D

TOWNSHIP : RANGE :

DATE : 06/22/95 PERMANENT DATUM : G.L. ELEVATIONS
DEPTH DRILLER : 400 ELEV. PERM. DATUM: KB :
LOG BOTTOM : 405.00 LOG MEASURED FROM: G.L. DF :
LOG TOP : 0.70 DRL MEASURED FROM: G.L. GL :

CASING DRILLER : . LOGGING UNIT : 7
CASING TYPE : . FIELD OFFICE : TEHACHAPI.CA
CASING THICKNESS: . RECORDED BY : K.KEMP

BIT SIZE : 8 BOREHOLE FLUID : CLAY-GEL FILE : PROCESSED
MAGNETIC DECL. : RM : TYPE : 9041A
MATRIX DENSITY : RM TEMPERATURE : LOG : 4
FLUID DENSITY : MATRIX DELTA T : PLOT : 1 5
NEUTRON MATRIX : FLUID DELTA T : THRESH: 3000
REMARKS :

DRILLED BY: MYERS BROS. HANFORD, CA

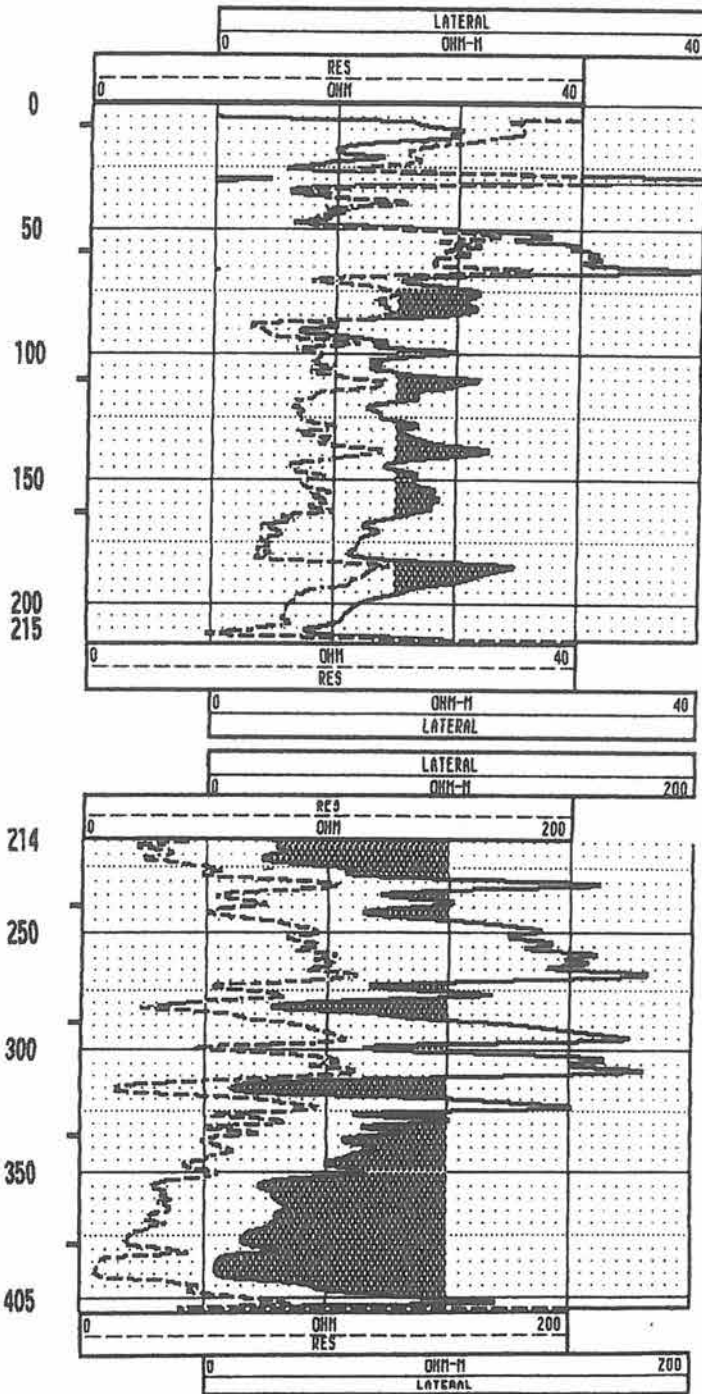
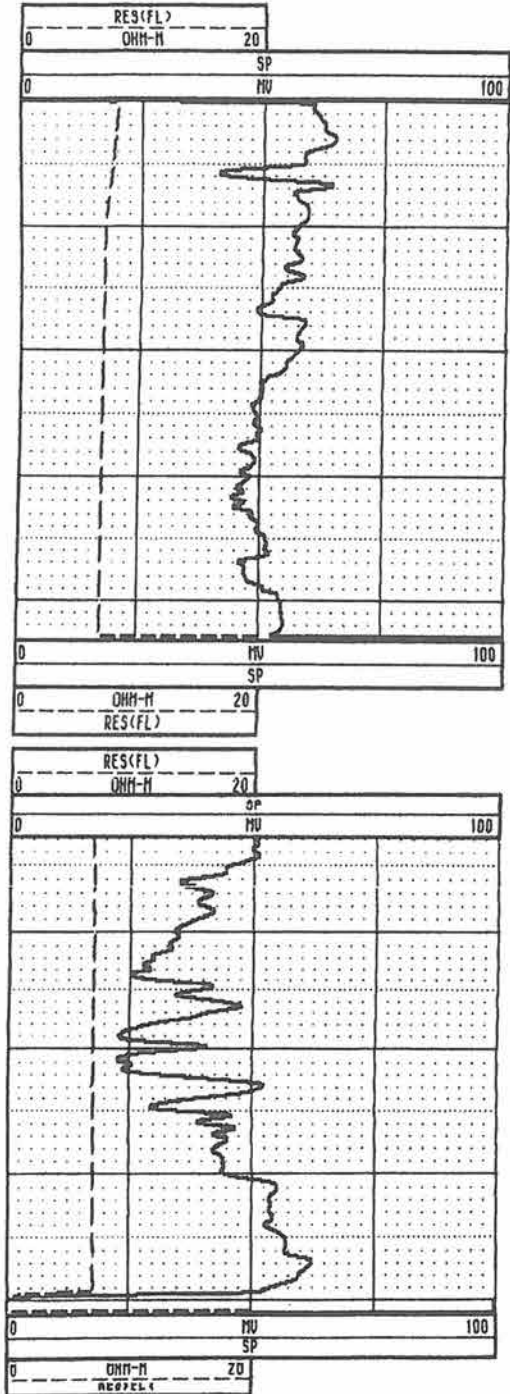
EXPECTED WATER QUALITY FAIR-POOR 900 TO 1,100 ppm TDS

ALL SERVICES PROVIDED SUBJECT TO STANDARD TERMS AND CONDITIONS

GEO-HYDRO-DATA

INCORPORATED

GROUNDWATER LOG



APPENDIX E

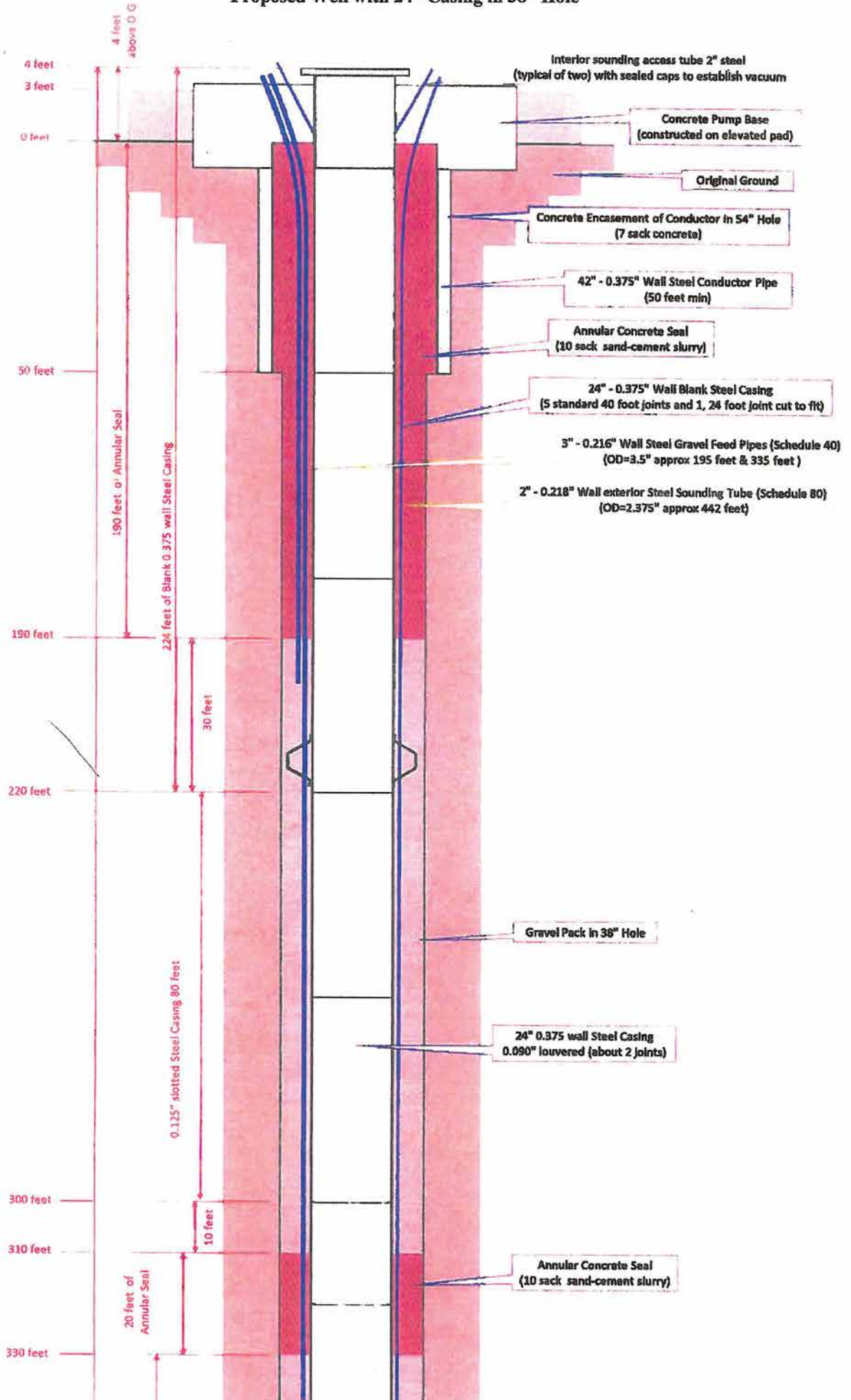
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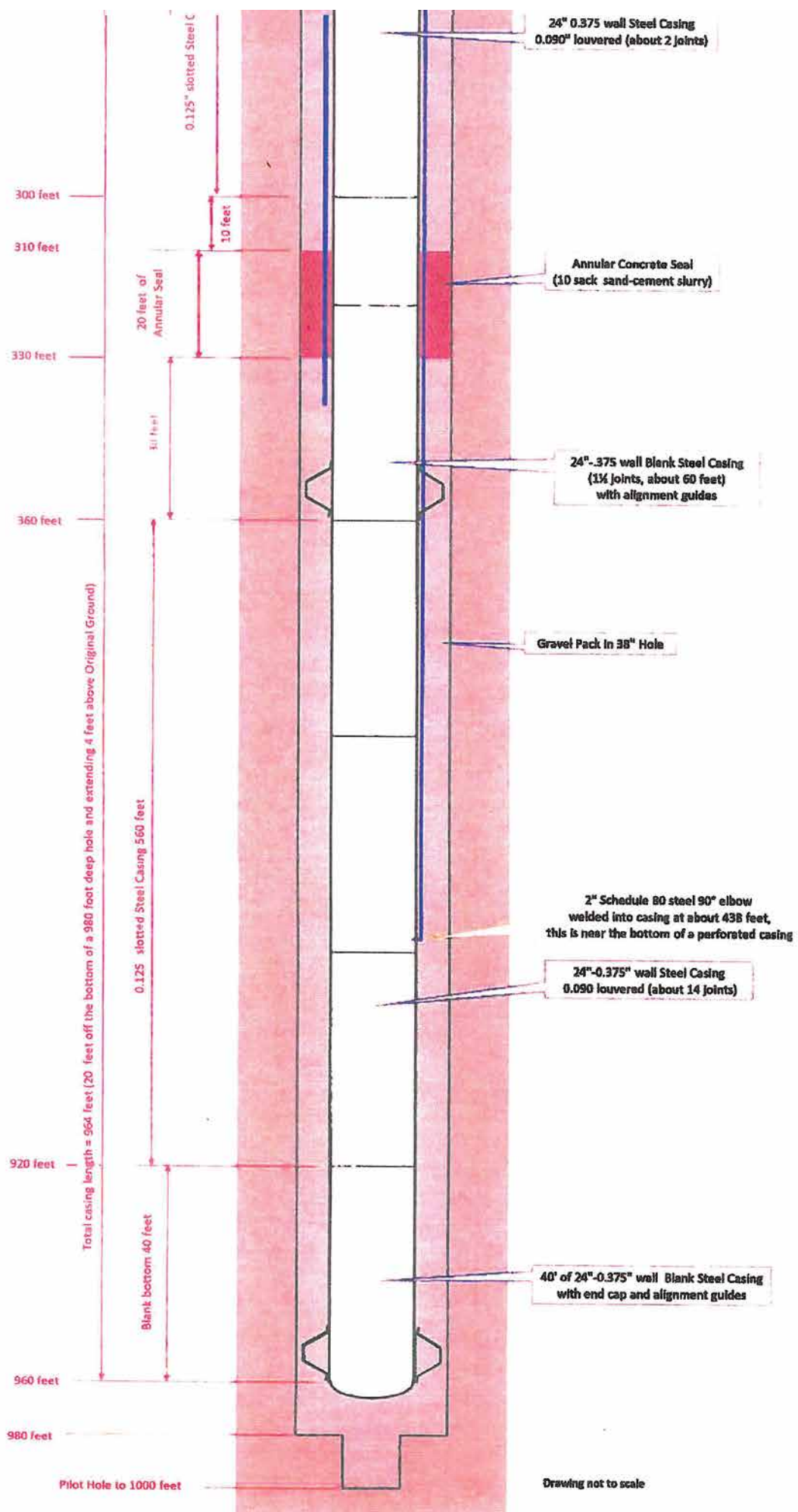
WELL SPECS

Source:
Appendix provided to Schrader Real Estate and
Auction Co., Inc. by the Owner.

OASIS RANCH

Proposed Well with 24" Casing in 38" Hole





Drawing not to scale



950 North Liberty Drive, Columbia City, IN 46725
800.451.2709 / 260.244.7606
www.schraderauction.com



California Real Estate Broker:
Clifford Crowe, Principal
Lee & Associates, Carlsbad, CA
License ID# 00982577